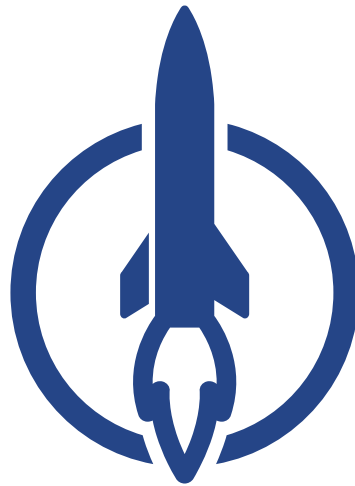


# EUROPEAN ROCKETRY CHALLENGE

## *DESIGN, TEST & EVALUATION GUIDE*



# EUROC

EUROPEAN ROCKETRY CHALLENGE



## INTERNAL APPROVAL

**PREPARED BY:**

Inês d'Ávila, Portuguese Space Agency  
Jacob Skov Larsen, Copenhagen Suborbitals  
Pedro Costa, Portuguese Space Agency  
Tiago Peres, Portuguese Space Agency

Signature:

Date: 06/03/2023

**VERIFIED BY:**

Inês d'Ávila, Portuguese Space Agency  
Marta Gonçalves, Portuguese Space Agency

Signature:

Date: 06/03/2023

**APPROVED BY:**

Ricardo Conde, Portuguese Space Agency

Signature:

Date: 06/03/2023



# TABLE OF CONTENTS

<b><u>LIST OF REVISIONS</u></b> .....	<b>7</b>
<b><u>1. INTRODUCTION</u></b> .....	<b>8</b>
<b><u>1.1. BACKGROUND</u></b> .....	<b>8</b>
<b><u>1.2. PURPOSE</u></b> .....	<b>8</b>
<b><u>1.3. DOCUMENTATION</u></b> .....	<b>10</b>
<b><u>2. PROPULSION SYSTEMS</u></b> .....	<b>10</b>
<b><u>2.1. NON-TOXIC PROPELLANTS</u></b> .....	<b>10</b>
<b><u>2.2. COTS SOLID MOTORS</u></b> .....	<b>11</b>
<b><u>2.3. IGNITION SYSTEMS FOR SOLID MOTORS</u></b> .....	<b>11</b>
<b><u>2.4. PROPULSION SYSTEM SAFING AND ARMING</u></b> .....	<b>11</b>
<b><u>2.4.1. GROUND-START IGNITION CIRCUIT ARMING</u></b> .....	<b>11</b>
<b><u>2.4.2. AIR-START IGNITION CIRCUIT ARMING</u></b> .....	<b>12</b>
<b><u>2.4.3. CLUSTERED PROPULSION</u></b> .....	<b>12</b>
<b><u>2.5. AIR-START IGNITION CIRCUIT ELECTRONICS</u></b> .....	<b>13</b>
<b><u>2.6. SRAD PROPULSION SYSTEMS</u></b> .....	<b>14</b>
<b><u>2.6.1. COMBUSTION CHAMBER PRESSURE TESTING</u></b> .....	<b>14</b>
<b><u>2.6.2. HYBRID AND LIQUID PROPULSION FILLING SYSTEMS</u></b> .....	<b>14</b>
<b><u>2.6.3. HYBRID AND LIQUID PROPULSION SYSTEM TANKING TESTING</u></b> .....	<b>14</b>
<b><u>2.6.4. HYBRID/LIQUID VENTING</u></b> .....	<b>15</b>
<b><u>2.6.5. PROPELLANT OFFLOADING AFTER LAUNCH ABORT</u></b> .....	<b>15</b>
<b><u>2.6.6. STATIC HOT-FIRE TESTING</u></b> .....	<b>15</b>
<b><u>3. RECOVERY SYSTEMS AND AVIONICS</u></b> .....	<b>16</b>
<b><u>3.1. DUAL-EVENT PARACHUTE AND PARAFOIL RECOVERY</u></b> .....	<b>16</b>
<b><u>3.1.1. INITIAL DEPLOYMENT EVENT</u></b> .....	<b>16</b>
<b><u>3.1.2. MAIN DEPLOYMENT EVENT</u></b> .....	<b>16</b>
<b><u>3.1.3. EJECTION GAS PROTECTION</u></b> .....	<b>16</b>
<b><u>3.1.4. PARACHUTE SWIVEL LINKS</u></b> .....	<b>17</b>
<b><u>3.1.5. PARACHUTE COLORATION AND MARKINGS</u></b> .....	<b>17</b>
<b><u>3.2. NON-PARACHUTE/PARAFOIL RECOVERY SYSTEMS</u></b> .....	<b>17</b>
<b><u>3.3. REDUNDANT ELECTRONICS</u></b> .....	<b>17</b>
<b><u>3.4. ON-BOARD POWER SYSTEMS AND RAIL STANDBY TIME</u></b> .....	<b>17</b>
<b><u>3.4.1. REDUNDANT COTS RECOVERY ELECTRONICS</u></b> .....	<b>19</b>



---

<u>3.4.2. DISSIMILAR REDUNDANT RECOVERY ELECTRONICS</u> .....	20
<u>3.4.3. RECOVERY ELECTRONICS ACCESS</u> .....	20
<u>3.4.4. ELECTRONICS RELIABILITY, STRESS TESTING AND OVER-HEATING</u> .....	20
<b><u>3.5. OFFICIAL ALTITUDE LOGGING AND TRACKING SYSTEM</u></b> .....	<b>21</b>
<u>3.5.1. CATS VEGA FLIGHT COMPUTER AS COTS FLIGHT COMPUTER FOR RECOVERY</u> .....	21
<u>3.5.2. CATS VEGA FLIGHT COMPUTER FREQUENCIES</u> .....	21
<u>3.5.3. CATS TRANSMITTER CALL-SIGN</u> .....	22
<u>3.5.4. CATS TRANSMITTER CALL-SIGN EXAMPLES</u> .....	22
<u>3.5.5. CATS VEGA FLIGHT COMPUTER FIRMWARE UPDATE</u> .....	23
<u>3.5.6. CATS RECEIVER</u> .....	23
<u>3.5.7. CATS ELECTRONICS ACCESS</u> .....	24
<b><u>3.6. SAFETY CRITICAL WIRING</u></b> .....	<b>24</b>
<u>3.6.1. CABLE MANAGEMENT</u> .....	24
<u>3.6.2. SECURE CONNECTIONS</u> .....	24
<u>3.6.3. CRYO-COMPATIBLE WIRE INSULATION</u> .....	24
<b><u>3.7. RECOVERY SYSTEM ENERGETIC DEVICES</u></b> .....	<b>24</b>
<b><u>3.8. RECOVERY SYSTEM TESTING</u></b> .....	<b>25</b>
<u>3.8.1. GROUND TEST DEMONSTRATION</u> .....	25
<u>3.8.2. OPTIONAL FLIGHT TEST DEMONSTRATION</u> .....	25
<u>3.8.3. OPTIONAL FLIGHT ELECTRONICS DEMONSTRATION</u> .....	26
<b><u>4. STORED-ENERGY DEVICES</u></b> .....	<b>26</b>
<b><u>4.1. ENERGETIC DEVICE SAFING AND ARMING</u></b> .....	<b>26</b>
<u>4.1.1. ARMING DEVICE ACCESS</u> .....	27
<u>4.1.2. ARMING DEVICE LOCATION</u> .....	27
<b><u>4.2. SRAD PRESSURE VESSELS</u></b> .....	<b>27</b>
<u>4.2.1. RELIEF DEVICE</u> .....	28
<u>4.2.2. DESIGNED BURST PRESSURE FOR METALLIC PRESSURE VESSELS</u> .....	28
<u>4.2.3. DESIGNED BURST PRESSURE FOR COMPOSITE PRESSURE VESSELS</u> .....	28
<u>4.2.4. SRAD PRESSURE VESSEL TESTING</u> .....	28
<b><u>5. ACTIVE FLIGHT CONTROL SYSTEMS</u></b> .....	<b>29</b>
<b><u>5.1. CONTROL FUNCTIONALITY</u></b> .....	<b>29</b>
<b><u>5.2. UNNECESSARY FOR STABLE FLIGHT</u></b> .....	<b>30</b>
<b><u>5.3. DESIGNED TO FAIL SAFE</u></b> .....	<b>30</b>
<b><u>5.4. BOOST PHASE DORMANCY</u></b> .....	<b>30</b>
<b><u>5.5. RECOMMENDED FLIGHT TRAJECTORY FOR ACTIVE CONTROL SYSTEMS</u></b> .....	<b>31</b>
<b><u>5.6. ACTIVE FLIGHT CONTROL SYSTEM ELECTRONICS</u></b> .....	<b>31</b>

---



---

<b>5.7. ACTIVE FLIGHT CONTROL SYSTEM ENERGETICS</b> .....	<b>32</b>
<b>6. AIRFRAME STRUCTURES</b> .....	<b>32</b>
<b>6.1. ADEQUATE VENTING</b> .....	<b>32</b>
<b>6.2. OVERALL STRUCTURAL INTEGRITY</b> .....	<b>32</b>
6.2.1. MATERIAL SELECTION.....	32
6.2.2. LOAD BEARING EYEBOLTS AND U-BOLTS.....	33
6.2.3. IMPLEMENTING COUPLING TUBES .....	33
6.2.4. LAUNCH LUG MECHANICAL ATTACHMENT.....	33
<b>6.3. RF TRANSPARENCY</b> .....	<b>34</b>
<b>6.4. IDENTIFYING MARKINGS</b> .....	<b>34</b>
<b>6.5. OTHER MARKINGS</b> .....	<b>34</b>
<b>7. PAYLOAD</b> .....	<b>35</b>
<b>7.1. PAYLOAD RECOVERY</b> .....	<b>35</b>
7.1.1. PAYLOAD RECOVERY SYSTEM ELECTRONICS AND SAFETY CRITICAL WIRING .....	35
7.1.2. PAYLOAD RECOVERY SYSTEM TESTING .....	35
7.1.3. DEPLOYABLE PAYLOAD LANDING SITE TRACKING REQUIRED .....	35
<b>7.2. PAYLOAD ENERGETIC DEVICES</b> .....	<b>36</b>
<b>8. LAUNCH AND ASCENT TRAJECTORY REQUIREMENTS</b> .....	<b>36</b>
<b>8.1. LAUNCH AZIMUTH AND ELEVATION</b> .....	<b>36</b>
<b>8.2. LAUNCH STABILITY AND ADEQUATE RAIL TAKE-OFF VELOCITY</b> .....	<b>36</b>
<b>8.3. ASCENT STABILITY</b> .....	<b>37</b>
<b>8.4. OVER-STABILITY</b> .....	<b>37</b>
<b>9. EUROC LAUNCH SUPPORT EQUIPMENT</b> .....	<b>37</b>
<b>9.1. LAUNCH RAILS</b> .....	<b>37</b>
9.1.1. LAUNCH RAIL FIT CHECK .....	39
<b>9.2. EUROC-PROVIDED LAUNCH CONTROL SYSTEM</b> .....	<b>40</b>
<b>10. TEAM-PROVIDED LAUNCH SUPPORT EQUIPMENT</b> .....	<b>40</b>
<b>10.1. EQUIPMENT PORTABILITY</b> .....	<b>40</b>
<b>10.2. LAUNCH RAIL ELEVATION</b> .....	<b>40</b>

---



<b><u>10.3. OPERATIONAL RANGE</u></b> .....	<b>40</b>
<b><u>10.4. FAULT TOLERANCE AND ARMING</u></b> .....	<b>40</b>
<b><u>10.5. SAFETY CRITICAL SWITCHES</u></b> .....	<b>41</b>
<b><u>APPENDIX A: ACRONYMS, ABBREVIATIONS &amp; TERMS</u></b> .....	<b>42</b>
<b><u>APPENDIX B: GRADING CRITERIA</u></b> .....	<b>43</b>
<b><u>APPENDIX C: FIRE CONTROL SYSTEM DESIGN GUIDELINES</u></b> .....	<b>49</b>
<b><u>APPENDIX D: FLIGHT READINESS REVIEW CHECKLIST</u></b> .....	<b>53</b>



## LIST OF REVISIONS

REVISION	DATE	DESCRIPTION
Version 01	20/07/2020	Original edition.
Version 02	03/03/2021	Second version, major revisions for EuRoC 2021.
Version 03	04/02/2022	Third version, major revisions for EuRoC 2022.
Version 04	20/02/2023	Fourth version, overall revisions for EuRoC 2023. Important revisions in Sections: 2.2. 3.4. 3.5. , 5., 8.2. 10.5. Appendix B:
Version 4.1	06/03/2023	Fourth version, revision 1: clarifications on Section 3.4. and references update.



# 1. INTRODUCTION

## 1.1. BACKGROUND

The Portuguese Space Agency – Portugal Space promotes the EuRoC – European Rocketry Challenge, a competition that seeks to stimulate university level students to fly sounding rockets, by designing and building the rockets themselves. It is widely recognized that such competitions foster innovation and motivate students to extend themselves beyond the classroom, while learning to work as a team, solving real world problems under the same pressures they will experience in their future careers.

EuRoC is fully aligned with the strategic goals of Portuguese Space Agency, namely the development and evolution of the cultural/educational internationalization frameworks capable of boosting the development of the Space sector in Portugal.

Since EuRoC's first edition, in 2020, where 100 students were present to 2022, with 500 students participating, the growth of the competition within Europe is visible, and especially within Portugal, with an increasing number of interested teams applying to the competition. For the future, it is the Portuguese Space Agency's goal to continue to foster the exchange of knowledge and international interaction inherent to the event, allowing more students to gain from the Challenge and, at the same time, contribute to it.

This document defines the rules and requirements governing participation in EuRoC. Major revisions of this document will be accomplished by complete document reissue. Smaller revisions will be reflected in updates to the document's effective date and marked by the revision number. The authority to approve and issue revised versions of this document rests with Portuguese Space Agency.

## 1.2. PURPOSE

This document defines the minimum design, test and evaluation criteria that teams must meet before launching at the competition. These criteria main goal is to promote flight safety. Departures from the guidance this document provides may negatively impact a team's score and flight status, depending on the degree of severity. The foundational, qualifying criteria for EuRoC are contained in the EuRoC Rules & Requirements document.

The following definitions differentiate between requirements and other statements. The degree to which a team satisfies the spirit and intent of these statements will guide the competition officials' decisions on a project's overall score in EuRoC and flight status at the competition.

### **Shall**

Denotes mandatory requirements.





Failure to satisfy the spirit and intent of a mandatory requirement will always affect a project's score and flight status negatively.

### **Should**

Denotes non-mandatory goals.

Failure to satisfy the spirit and intent of a non-mandatory goal may affect a project's score and flight status, depending on design implementation and the team's ability to provide thorough documentary evidence of their due diligence on-demand.

Compliance to recommended goals and requirements may impact a team's score and flight status in a positive way, as demonstrating additional commitment and diligence to implement (often safety and reliability related guidelines) is commendable.

### **Will**

States facts and declarations of purpose.

These statements are used to clarify the spirit and intent of requirements and goals.

### **Flight status**

Refers to the granting of permission to attempt a launch and the provisions under which that permission remains valid.

A project's flight status may be either nominal, provisional, or denied. The default flight status of any team is from the project onset "denied", until project deliverables, and ultimately a successful Flight Readiness Review and Flight Safety Review, convinces the EuRoC officials to upgrade the flight status of teams.

1) Nominal:

- A project assigned nominal flight status meets or exceeds the minimum expectations of this document and reveals no obvious flight safety concerns during flight safety review at the competition.

2) Provisional:

- A project assigned provisional flight status generally meets the minimum expectations of this document but reveals flight safety concerns during flight safety review at the competition which may be mitigated by field modification or by adjusting launch environment constraints. Launch may occur only when the prescribed provisions are met.

3) Denied:

- Competition officials reserve the right to deny flight status to any project which fails to meet the minimum expectations of this document or reveals un-mitigatable flight safety concerns during flight safety review at the competition.



An effort is made throughout this document to differentiate between launch vehicle and payload associated systems. Unless otherwise stated, requirements referring only to the launch vehicle do not apply to payloads and vice versa.

### 1.3. DOCUMENTATION

The following documents include standards, guidelines, schedules, or required standard forms. The documents listed in this section (Table 1) are either applicable to the extent specified herein or contain reference information useful in the application of this document.

*Table 1: Documents file location.*

<i>DOCUMENT</i>	<i>FILE LOCATION</i>
EuRoC Rules & Requirements	<a href="http://www.euroc.pt">http://www.euroc.pt</a>
EuRoC Design, Test & Evaluation Guide	<a href="http://www.euroc.pt">http://www.euroc.pt</a>
EuRoC Launch Operations Guide	<a href="http://www.euroc.pt">http://www.euroc.pt</a>
EuRoC Entry Form	<a href="http://www.euroc.pt">http://www.euroc.pt</a>
EuRoC Academic Institution Participation Letter	<a href="http://www.euroc.pt">http://www.euroc.pt</a>
EuRoC Motors List	<a href="http://www.euroc.pt">http://www.euroc.pt</a>
EuRoC COTS Motors Acquisition Guide	<a href="http://www.euroc.pt">http://www.euroc.pt</a>
EuRoC Technical Questionnaire	<a href="http://www.euroc.pt">http://www.euroc.pt</a> (Teams' Reserved Area)
EuRoC Waiver and Release of Liability Form	<a href="http://www.euroc.pt">http://www.euroc.pt</a> (Teams' Reserved Area)
EuRoC Flight Card and Postflight Record	<a href="http://www.euroc.pt">http://www.euroc.pt</a> (Teams' Reserved Area)

## 2. PROPULSION SYSTEMS

### 2.1. NON-TOXIC PROPELLANTS

Launch vehicles entering EuRoC shall use non-toxic propellants. Ammonium perchlorate composite propellant (APCP), potassium nitrate and sugar (also known as "rocket candy"), nitrous oxide, liquid oxygen (LOX), hydrogen peroxide, kerosene, propane, alcohol, and similar substances, are all considered non-toxic. Toxic propellants are defined as those requiring breathing apparatus, unique storage and transport infrastructure, extensive personal protective equipment (PPE), etc. Home-made propellant mixtures containing any fraction of toxic propellants are also prohibited.



## 2.2. COTS SOLID MOTORS

Only COTS solid motors from the official EuRoC Motors List, compiled in conjunction with European suppliers, are permitted at EuRoC. More information on the motor acquisition process can be found in the EuRoC COTS Motors Acquisition Guide, available on the EuRoC website.

**Note:** Due to changes in US regulations as well as shortages in materials and substances, leading to abnormal long waiting times, the available COTS motors for the 2023 edition of EuRoC will be limited. As an attempt to address this issue, the COTS acquisition process might differ from the one specified in the EuRoC Rules & Requirements document. Teams can find more information in the EuRoC Motors List and COTS Motors Acquisition Guide, available on the EuRoC website.

## 2.3. IGNITION SYSTEMS FOR SOLID MOTORS

For all solid motors (COTS and SRAD), the use of the electronic ignition system provided by the EuRoC organisers is mandatory.

## 2.4. PROPULSION SYSTEM SAFING AND ARMING

A propulsion system is considered armed if only one action (e.g., an ignition signal) must occur for the propellant(s) to ignite. The "arming action" is usually something (i.e., a switch in series) that enables an ignition signal to ignite the propellant(s). For example, a software-based control circuit that automatically cycles through an "arm function" and an "ignition function" does not, in fact, implement arming. In this case, the software's arm function does not prevent a single action (e.g., starting the launch software) from causing unauthorized ignition. This problem may be avoided by including a manual interrupt in the software program.

These requirements generally concern more complex propulsion systems (i.e., hybrid, liquid, and multistage systems) and all team provided launch control systems. Additional requirements for team provided launch control systems are defined in Section 10. of this document.

### 2.4.1. GROUND-START IGNITION CIRCUIT ARMING

All ground-started propulsion system ignition circuits/sequences shall not be "armed" until all personnel are at least 15 m away from the launch vehicle. The provided launch control system satisfies this requirement by implementing a removable "safety jumper" in series with the pad relay box's power supply. The removal of this single jumper prevents firing current from being sent to any of the launch rails associated with that pad relay box. Furthermore, access to the socket allowing insertion of the



jumper is controlled via multiple physical locks to ensure that all parties have positive control of their own safety.

#### **2.4.2. AIR-START IGNITION CIRCUIT ARMING**

All upper stage (i.e., air-start) propulsion systems shall be armed by launch detection (e.g., accelerometers, zero separation force [ZSF] electrical shunt connections, break-wires, or other similar methods). Regardless of implementation, this arming function will prevent the upper stage from arming in the event of a misfire.

#### **2.4.3. CLUSTERED PROPULSION**

Partial ignition may occur in clustered propulsion systems, leading to an increased probability of incident occurrence, mainly by three potential consequences:

1. The thrust force is lower than expected, thus acceleration on the launch rail and resulting launch rail take-off velocity too low, leading to an unstable flight.
2. The thrust force asymmetric, leading to a sideways momentum on the rocket off the launch rail, thus to an unstable flight, and potentially a structural failure.
3. Incompletely ignited propulsion systems separate from the vehicle, ignite in the air, or ignite from the top, and burning parts impact the ground.

To ensure stable flight, all clustered vehicles shall have a launch release system ensuring lift-off only occurs if a minimum threshold force is met. This can be done for example by implementing a breakaway coupling, a structural fuse, or a rope with defined breaking force.

An electromechanical alternative to a structural fuse is to measure the thrust of the restrained flight vehicle and then open a quick release mechanism if certain conditions are fulfilled. For example, as the vehicle throttles up, a squib/pyro actuated quick release latch can be electrically fired (i.e., Sweeney quick release latch) when the thrust has continuously exceeded a minimum threshold for perhaps 200 milliseconds (jerk and noise suppression).



*Figure 1: Example of a Sweeney quick release latch.  
(Source: Matt Sweeney SPFX Inc.)*

To measure the thrust, a strain gauge could be used, or alternatively piezoelectric pressure sensors can be applied to measure the combustion pressure inside a thrust chamber, verifying that nominal thrust has been achieved before the quick release squib is fired. If the latter method with pressure sensors is used, the sensor/transducer shall be of stainless-steel and mounted in a way so that it remains protected from hot combustion gases by means of an oil trap.

Furthermore, all clustered vehicles shall provide an engineering proof (e.g., analysis and/or simulation) that stable flight is ensured for a lift-off force above the threshold force, even if the propulsion system fires asymmetrically (if applicable).

For vehicles with a “main” and several “secondary” propulsion systems, the arming function of the secondary propulsion systems shall be armed by launch detection (i.e., air-start), preventing ground arming of the clustered propulsion in event of misfire.

## 2.5. AIR-START IGNITION CIRCUIT ELECTRONICS

All upper stage ignition systems shall comply with the same requirements and goals for "redundant electronics" and "safety critical wiring" as recovery systems — understanding that in this case "initiation" refers to upper stage ignition rather than a recovery event. These requirements and goals are defined in Sections 3.3. . and 3.6. . respectively.



## 2.6. SRAD PROPULSION SYSTEMS

Teams shall comply with all rules, regulations, and best practices imposed by the authorities at their chosen test location(s). The following requirements concern verification testing of student researched and developed (SRAD) and modified commercial-off-the-shelf (COTS) propulsion systems.

### 2.6.1. COMBUSTION CHAMBER PRESSURE TESTING

SRAD and modified COTS propulsion system combustion chambers shall be designed and tested according to the SRAD pressure vessel requirements defined in Section 4.2. .. Note that combustion chambers are exempted from the requirement for a relief device.

### 2.6.2. HYBRID AND LIQUID PROPULSION FILLING SYSTEMS

Teams shall demonstrate that the filling/loading/unloading of the liquid fuels can be done to be ready for the launch window (maximum 90 minutes for liquid propellant loading, including pressurization).

Teams utilising liquid propellants with low boiling point are also strongly encouraged to consider abandoning the use of “passive” or “self-pressurization” of propellants and adopt active external or internal pressurization (nitrogen or helium). Besides removing the significant propellant density uncertainties of two-phase flows (a volatile and somewhat arbitrary mixture of gas bubbles and liquid) in injectors, the flight vehicle can be pressurized in typically less than 15 seconds, at any point in time after having been loaded on the launch rail.

If teams utilise any kind of remote-controlled loading mechanism for gases or liquid propellants, the loading mechanism shall feature a clearly marked and labelled, single action, hand actuated, “Emergency Release Mechanism”, just in case a remote-controlled release mechanism jams and requires manual LCO (Launch Control Officer) assistance.

It is strongly recommended that the flight vehicle is designed such that any filling/loading/unloading connections for fluid propellants are readily accessible from the ground. No propellant loading procedure should necessitate ladders or other elevation devices. Furthermore, teams should account for a “failed” launch and subsequent unloading in launch preparation, thus teams should ensure the availability of additional propellants, igniters, and any other parts that might need replacement or adjustment in case a second launch attempt would be possible.

### 2.6.3. HYBRID AND LIQUID PROPULSION SYSTEM TANKING TESTING

SRAD and modified COTS propulsion systems using liquid propellant(s) shall successfully (without significant anomalies) have completed a propellant loading and off-loading test in “launch-configuration”, prior to the rocket being brought to the competition. This test may be conducted using



either actual propellant(s) or suitable proxy fluids, with the test results to be considered a mandatory deliverable and an annex to the Technical Report, in the form of a loading and off-loading checklist, complete with dates, signatures (at least three) and a statement of a successful test. Referring to Section 2.6.6. , it is highly recommended to perform this test multiple times as part of the “all-up static engine test” configuration, described in that section.

The described annex may be amended to the Technical Report, as results become available, up to the day final deadline for delivery of the Technical Report. Failure to deliver this annex will automatically result in a “denied” flight status.

Loading and unloading of liquid propellants must be a well-drilled, safe and efficient operation at the competition launch rails.

#### **2.6.4. HYBRID/LIQUID VENTING**

For hybrid and liquid motors, it is imperative that teams can facilitate oxidizer tank venting to prevent over-pressure situations. Teams will only be able to launch in specific time slots, so pressure relief measures shall be implemented to account for rockets potentially sitting a long time in waiting on the launch rail. At no time must oxidizer tanks become safety liabilities.

#### **2.6.5. PROPELLANT OFFLOADING AFTER LAUNCH ABORT**

Hybrid and liquid propulsion systems shall implement a means for remotely controlled venting or offloading of all liquid and gaseous propellants in the event of a launch abort.

#### **2.6.6. STATIC HOT-FIRE TESTING**

SRAD propulsion systems shall successfully (without significant anomalies) complete an instrumented (chamber pressure and/or thrust), full scale (including system working time) static hot-fire test prior to EuRoC. In the case of solid rocket motors, this test needs not to be performed with the same motor casing and/or nozzle components intended for use at the EuRoC (i.e., teams must verify their casing design, but are not forced to design reloadable/reusable motor cases).

The test shall, to the extent possible, be conducted as an “all-up static engine test”, which means that the completed flight vehicle, rigidly fastened to a suitable test stand in an upright position, should be tested for a full duration burn under the most realistic settings possible. Test results from horizontal tests, using flight components is less optimum, whereas test results from test benches (not using flight components) do not qualify.

The test results and a statement of a successful test, complete with dates and signatures (at least three) are considered a mandatory deliverable and an annex to the Technical Report.



The described annex may be amended to the Technical Report, as results become available, up to the day final deadline for delivery of the Technical Report. Failure to deliver this annex will automatically result in a “denied” flight status.

“Test as you fly – Fly as you test”. This test-mentality significantly increases the chances of a lift-off and a nominal flight.

## **3. RECOVERY SYSTEMS AND AVIONICS**

### **3.1. DUAL-EVENT PARACHUTE AND PARAFOIL RECOVERY**

Each independently recovered launch vehicle body, anticipated to reach an apogee above 450 m above ground level (AGL), shall follow a "dual-event" recovery operations concept, including an initial deployment event (e.g., a drogue parachute deployment; reefed main parachute deployment or similar) and a main deployment event (e.g., a main parachute deployment; main parachute un-reefing or similar). Independently recovered bodies, whose apogee is not anticipated to exceed 450 m AGL, are exempt and may feature only a single/main deployment event.

#### **3.1.1. INITIAL DEPLOYMENT EVENT**

The initial deployment event shall occur at or near apogee, stabilize the vehicle's attitude (i.e., prevent or eliminate tumbling), and reduce its descent rate sufficiently to permit the main deployment event, yet not so much as to exacerbate wind drift. Any part, assembly or device, featuring an initial deployment event, shall result in a descent velocity of said item of 23-46 m/s.

#### **3.1.2. MAIN DEPLOYMENT EVENT**

The main deployment event shall occur at an altitude no higher than 450 m AGL and reduce the vehicle's descent rate sufficiently to prevent excessive damage upon impact with ground. Any part, assembly or device, featuring a main deployment event, shall result in a descent velocity of said item of less than 9 m/s.

#### **3.1.3. EJECTION GAS PROTECTION**

The recovery system shall implement adequate protection (e.g., fire-resistant material, pistons, baffles etc.) to prevent hot ejection gases (if implemented) from causing burn damage to retaining chords, parachutes, and other vital components as the specific design demands.





### **3.1.4. PARACHUTE SWIVEL LINKS**

The recovery system rigging (e.g., parachute lines, risers, shock chords, etc.) shall implement swivel links at connections to relieve torsion, as the specific design demands. This will mitigate the risk of torque loads unthreading bolted connections during recovery as well as parachute lines twisting up.

### **3.1.5. PARACHUTE COLORATION AND MARKINGS**

When separate parachutes are used for the initial and main deployment events, these parachutes should be visually highly dissimilar from one another. This is typically achieved by using parachutes whose primary colours contrast those of the other chute. This will enable ground-based observers to characterize deployment events more easily with high-power optics.

Utilised parachutes should use colours providing a clear contrast to a blue sky and a grey/white cloud cover.

## **3.2. NON-PARACHUTE/PARAFOIL RECOVERY SYSTEMS**

Teams exploring other recovery methods (i.e., non-parachute or parafoil based) shall mention them in the dedicated field of the Technical Questionnaire (see Section 9.1. of the EuRoC Rules & Requirements document). The organisers may make additional requests for information and draft unique requirements depending on the team's specific design implementation.

## **3.3. REDUNDANT ELECTRONICS**

Launch vehicles shall implement redundant recovery system electronics, including sensors/flight computers and "electric initiators" — assuring initiation by a backup system, with a separate power supply (i.e., battery), if the primary system fails. In this context, electric initiators are the devices energized by the sensor electronics, which then initiates some other mechanical or chemical energy release, to deploy its portion of the recovery system (i.e., electric matches, nichrome wire, flash bulbs, etc.).

## **3.4. ON-BOARD POWER SYSTEMS AND RAIL STANDBY TIME**

Lithium-Polymer (LiPo) batteries are not allowed due to the increased flammability and thus an increased fire hazard. Teams shall implement less flammable on-board power systems. Below teams can find the battery general prioritisation, and allowed characteristics, according to toxicity, flammability, environmental hazards, etc).



1. LiFePO<sub>4</sub> chemistry cells are allowed in any form factor and in any casing (plastic or metallic).
2. NiMH (Nickel-Metalhydride) chemistry cells are allowed in metal casing and any form factor.
3. Alkaline chemistry (non-rechargeable) cells are allowed in metal casing and any form factor. External power may be provided to a rocket via umbilical cable, to avoid draining alkaline (non-rechargeable) batteries while sitting on the launch rail.
4. Other Li-Ion chemistry cells are allowed, but shall be of metallic casing cylindrical form factor, which provides increased ruggedness against mechanical damage. Li-Ion cells in rectangular form factor and/or plastic casing are prohibited.

LiPo (Lithium-polymer) cells are prohibited, regardless of encapsulation or form factor. These cells have negligible mechanical resilience, low ignition temperature and an exothermic decomposition nature. Lithium chemistry (non-rechargeable) cells are prohibited, regardless of encapsulation or form factor, due to the high probability of metallic Lithium, REACH concerns or toxicity/environmental impact.

**Note:** This requirement only applies to the on-board systems, off-board systems are exempt of such requirement.

Loss of launch slots have been experienced on multiple occasions as onboard batteries are typically located in inaccessible positions. Despite the requirement of at least six hours of battery life on the launch rail, an unsuccessful launch attempt typically results in the teams deciding to:

- Disarm any energetic pyrotechnics;
- Take the flight vehicle off the launch rail;
- Haul the rocket back to the team's preparation area;
- Use tools to perform medium to extensive disassembly of the flight vehicle to extract batteries;
- Spend one to several hours recharging the batteries, if charged spares are not readily available;
- Perform the whole operation in reverse and return to the launch rail many hours later, to perform an additional launch attempt, if the possibility is given.

This is a critically inefficient use of valuable and limited launch campaign time.

Teams should adopt one of the following two strategies:

- Implement an on-board charging and charge level maintenance system using an umbilical connection and cable;
- Place all rechargeable or replaceable batteries conveniently under service panels accessible from ground level, without resorting to ladders or lowering the launch rail, having several spare sets of charged batteries ready at any time.

The implementation of an on-board charging and charge level maintenance system, based on a vehicle-wide charging bus and an umbilical cable (featuring friction-based pull-release), connected to a ground-based power supply, should be designed/implemented as follows:



- A “charging bus” should run along the entire length of the flight vehicle, interfacing to all batteries to facilitate charging and continuous charging and subsequent maintenance trickle-charging;
  - Use mating connectors at every structural joint;
  - Largely all benefits of the system are lost if even a single battery is left out of the umbilical charging bus system.
- Each tap-off from the on-board charging bus to individual battery subsystems shall be reverse current flow protected by a suitably rated diode;
- All on-board batteries should feature the same nominal voltage, as far as possible;
  - If bus voltage step-down is required for batteries with lower nominal voltage, adequately heat-dissipated linear regulators are recommended and placed upstream of the mandatory cell balancing circuits, since they bypass any EMI issues inherent to switching DC-DC converters;
  - Switch-mode regulation or onboard battery chargers require acute attention to generated EMI and electrical noise;
  - Flight vehicle batteries could all be considered “permanently” installed, not requiring removal past initial installation during on-site preparation. The ground-based power supply should simply be outputting the battery trickle charge voltage, plus a diode drop, for easiest implementation.

The advantages of implementing such a system are in most cases worth the efforts. Most significantly, the launch vehicle rail standby time changes to “infinite” and the launch vehicle is always launched with 100% peak charged batteries.

### 3.4.1. REDUNDANT COTS RECOVERY ELECTRONICS

At least one redundant recovery system electronics subsystem shall implement a COTS flight computer (e.g., StratoLogger, G-Wiz, Raven, Parrot, Eggtimer, AIM, EasyMini, TeleMetrum, RRC3, CATS, etc.).

To be considered COTS, the flight computer (including flight software) must have been developed and validated by a commercial third party. While commercially designed flight computer “kits” (e.g., the Eggtimer) are permitted and considered COTS, any student developed flight computer assembled from separate COTS components will not be considered a COTS system. Similarly, any COTS microcontroller running student developed flight software will not be considered a COTS system. Any SRAD hardware implemented between a COTS flight computer and any recovery system actuator (e.g., servo, e-match, thermal knife, solenoid valve, nicrome wire, or similar) violates the redundant COTS recovery electronics requirement, resulting in a denied flight status.

The interconnection redundancy of the nominal and redundant recovery electronics and recovery systems should be implemented as illustrated in Figure 2.

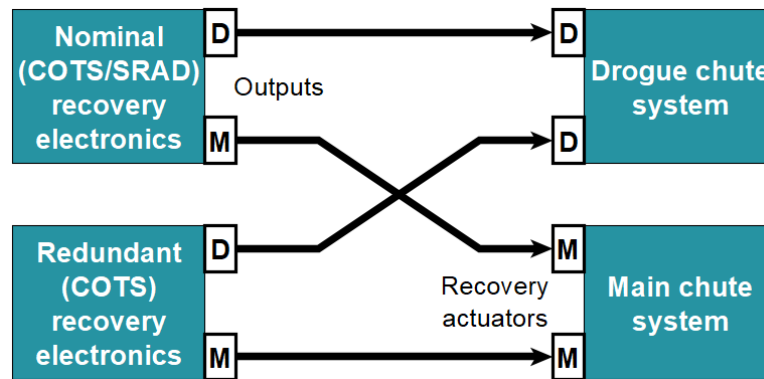


Figure 2: Interconnection redundancy implementation. (Source: Jacob Larsen)

### 3.4.2. DISSIMILAR REDUNDANT RECOVERY ELECTRONICS

There is no requirement that the redundant/backup system be dissimilar to the primary; however, there are advantages to using dissimilar primary and backup systems. Such configurations are less vulnerable to any inherent environmental sensitivities, design, or production flaws affecting a particular component.

### 3.4.3. RECOVERY ELECTRONICS ACCESS

As for all electronics, it is highly recommended to ensure easy and quick access to switches/connectors via an access panel on the airframe. Access panels should be positioned so they are reachable from ground level, ideally without ladders. Access panels shall be secured for flight.

### 3.4.4. ELECTRONICS RELIABILITY, STRESS TESTING AND OVER-HEATING

Experience from prior EuRoC events reveal that electronics problems account for an estimated 70% of cases where teams experience unreliable electronics, loss of telemetry, loss of control or other anomalies, which often leads to scrubbed launches or even loss of the flight vehicle.

One clear trend is that teams fail to take action on conducting proper thermal testing of their electronics and/or adding suitable cooling or venting provisions.

While electronics tend to work well in a temperature-controlled laboratory environment, with open electronics compartments due to integration and testing, it must be taken into account that the flight vehicle may stay on a launch rail for several hours exposed to direct sun and high temperatures, with closed electronics compartments. In addition, when teams use black coloration, it results in maximum thermal absorption.



It is strongly recommended that teams thermally test their electronics to know the reliable operational temperature range, implement cooling or venting provisions and monitor at least one temperature sensor representative of the electronics temperature.

### 3.5. OFFICIAL ALTITUDE LOGGING AND TRACKING SYSTEM

Single-stage flight vehicles and upper-most stages of flight vehicles shall feature a mandatory operational CATS Vega Flight Computer for official altitude logging and landing site tracking. For more details see <https://catsystems.io>.

The competition achieved apogee will be determined from this device.

**Note:** Deployable payloads and lower stages also require a mandatory CATS Vega flight computer for landing site tracking purposes.

More technical details on the CATS Vega Flight Computer along with recommendations can be found in the CATS User Manual, available on the EuRoC website.

The CATS Vega Flight Computer system serves two purposes:

- Providing the EuRoC evaluation board with the means to easily determine and record the apogee altitude in a fast, efficient, and consistent way. Since the flight vehicle apogee is a fundamental part of the competition, the method of determining it must be equally fair (hence identical) for all teams;
- Provide the student/recovery teams an efficient means of quickly tracking down the location of all landed flight vehicles (and any other tracked payload/components), to quickly clear the launch range.

#### 3.5.1. CATS VEGA FLIGHT COMPUTER AS COTS FLIGHT COMPUTER FOR RECOVERY

The CATS Vega Flight Computer may be used as the COTS flight computers to comply with the requirements for redundant COTS Recovery Electronics according to section 3.3. ., or it may be used as an additional, independent standalone system for altitude logging and/or tracking purposes only.

It is recommended that teams evaluate the specifications and functionality of the system before deciding between implementing it as the main flight computer, redundant flight computer or leaving it entirely as a passive standalone “payload” (cargo).

#### 3.5.2. CATS VEGA FLIGHT COMPUTER FREQUENCIES

The CATS Vega system operates on the 2,4 GHz ISM band, with an EuRoC operating band allowed between 2.400 and 2.483,5 MHz and a maximum transmission power of 100 mW.



More information on the CATS system specifications can be found in the CATS User Manual, available on the EuRoC website.

### 3.5.3. CATS TRANSMITTER CALL-SIGN

Teams shall assign to each transmitter a “call-sign” (referred to in the CATS User Manual as the `tele_link_phrase` telecommand) respecting the following string format (case sensitive and no white-spaces allowed):

- Two-digit team number:
  - [xx]
- One underscore:
  - [ \_ ]
- Stage or (deployable) payload designation, depending on where the CATS device is mounted:
  - [stage] or [payload]
- Designation of stage or payload number, the first instance of each by default enumerated as “1”:
  - [y]
- Designation of the mandatory CATS flight computer in each stage or payload (with mandated EuRoC firmware version) is by default [m] and any additional CATS flight computer in the same stage or payload [a]:
  - [m] or [a]

Mission Control and Recovery units will by default lock on to [m] call-signs for flight- and recovery telemetry.

Teams should expect to be required to functionally demonstrate all CATS flight computer → CATS Ground station telemetry links of their flight vehicle during the Flight Readiness Review, as well as observe the Technical Evaluation Board representatives verify functional telemetry reception with separate TEB Ground stations.

### 3.5.4. CATS TRANSMITTER CALL-SIGN EXAMPLES

The following example is the CATS system call-sign applicable to Team 04, having a simple single stage rocket (one mandatory CATS unit, one additional COTS Altimax flight computer, and an internal dummy mass payload):

- 04\_stage1m

Next, Team 06, single-stage, mandatory CATS, additional SRAD flight computer, deployable payload with one mandatory CATS:

- 06\_stage1m



- 06\_payload1m

Team 20, single-stage, SRAD (primary recovery), mandatory CATS (flown as internal cargo), additional CATS (redundant recovery), deployable payload with mandatory CATS and additional CATS for deployable payload recovery redundancy:

- 20\_stage1m
- 20\_stage1a
- 20\_payload1m
- 20\_payload1a

Lastly, Team 22, having a two-stage rocket with two deployable payloads (both ejected from 2<sup>nd</sup> stage), constituting four mandatory and two additional CATS flight computers in total:

- 22\_stage1m
- 22\_stage1a
- 22\_stage2m
- 22\_stage2a
- 22\_payload1m
- 22\_payload2m

Please note that referring to section 3.5. all stages and deployable payloads require one mandatory CATS flight computer each, for uppermost stage altitude logging and landing point tracking of all landed ejected or jettisoned parts, enabling flight vehicle and payload recovery operations requiring a single CATS ground station. Additional CATS units (or any other flight computer(s)) in stages or payloads are optional, as are additional CATS ground stations.

### 3.5.5. CATS VEGA FLIGHT COMPUTER FIRMWARE UPDATE

Information on the CATS Vega firmware update procedure can be found in the CATS User Manual, available on the EuRoC website.

While the CATS Vega system is open-source, teams will be required to fly a specific firmware version in each mandatory CATS flight computer, mandated by the EuRoC organization. The EuRoC firmware version requirement still applies to CATS flight computers, regardless of if flown as inert “cargo” (no interfaces to any part of the recovery system) or as the mandatory COTS flight computer.

CATS flight computers not featuring the mandated EuRoC firmware version will be considered SRAD flight computers.

### 3.5.6. CATS RECEIVER

The CATS Ground Station is the supplementary hardware to the CATS Vega flight computer. Information on the CATS Ground Station can be found in the CATS User Manual, available on the EuRoC website.



### **3.5.7. CATS ELECTRONICS ACCESS**

As for all electronics, it is highly recommended to ensure easy and quick access to switches/connectors to on-board CATS devices via an access panel in the airframe. Access panels should ideally be positioned so they are reachable from ground level, without ladders. Access panels shall be secured for flight.

## **3.6. SAFETY CRITICAL WIRING**

For the purposes of this document, safety critical wiring is defined as electrical wiring associated with recovery system deployment events and any "air started" rocket motors.

### **3.6.1. CABLE MANAGEMENT**

All safety critical wiring shall implement a cable management solution (e.g., wire ties, wiring, harnesses, cable raceways) which will prevent tangling and excessive free movement of significant wiring/cable lengths due to expected launch loads. This requirement is not intended to negate the small amount of slack necessary at all connections/terminals to prevent unintentional de-mating due to expected launch loads transferred into wiring/cables at physical interfaces.

### **3.6.2. SECURE CONNECTIONS**

All safety critical wiring/cable connections shall be sufficiently secure as to prevent de-mating due to expected launch loads. This will be evaluated by a "tug test", in which the connection is gently but firmly "tugged" by hand to verify it is unlikely to break free in flight.

### **3.6.3. CRYO-COMPATIBLE WIRE INSULATION**

In case of propellants with a boiling point of less than  $-50^{\circ}\text{C}$  any wiring or harness passing within close proximity of a cryogenic device (e.g., valve, piping, etc.) or a cryogenic tank (e.g., a cable tunnel next to a LOX tank) shall utilize safety critical wiring with cryo-compatible insulation (i.e., Teflon, PTFE, etc.).

## **3.7. RECOVERY SYSTEM ENERGETIC DEVICES**

All stored-energy devices (i.e., energetics) used in recovery systems shall comply with the energetic device requirements defined in Section 4. of this document.





## 3.8. RECOVERY SYSTEM TESTING

Recovery system testing has proven to be one of the most critical and at the same time underestimated tasks. Teams are strongly encouraged to test the system back-to-back as well as they can and implement standard procedures that they can fall back onto even during the most stressful launch days.

Teams shall comply with all rules, regulations, and best practices imposed by the authorities at their chosen test location(s). The following requirements concern verification testing of all recovery systems.

### 3.8.1. GROUND TEST DEMONSTRATION

All recovery system mechanisms shall be successfully (without significant anomalies) tested prior to EuRoC, either by flight testing, or through one or more ground tests of key subsystems. In the case of such ground tests, sensor electronics will be functionally included in the demonstration by simulating the environmental conditions under which their deployment function is triggered.

The test results and a statement of a successful test, complete with dates and signatures (at least three) are considered a mandatory deliverable and annex to the Technical Report.

The described annex may be amended to the Technical Report, as results become available, up to the day final deadline for delivery of the Technical Report. Failure to deliver this annex will automatically result in a “denied” flight status.

Correct, reliable and repeatable recovery system performance is absolute top priority from a safety point of view. Statistical data also concludes that namely recovery system failures are the major cause of abnormal “landings”.

### 3.8.2. OPTIONAL FLIGHT TEST DEMONSTRATION

All recovery system mechanisms shall be successfully (without significant anomalies) tested prior to EuRoC, either by flight testing, or through one or more ground tests of key subsystems. While not required, a flight test demonstration may be used in place of ground testing. In the case of such a flight test, the recovery system flown will verify the intended design by implementing the same major subsystem components (e.g., flight computers and parachutes) as will be integrated into the launch vehicle intended for EuRoC (i.e., a surrogate booster may be used).

The test results and a statement of a successful test, complete with dates and signatures (at least three) are considered a mandatory deliverable and annex to the Technical Report.

The described annex may be amended to the Technical Report, as results become available, up to the day final deadline for delivery of the Technical Report. Failure to deliver this annex will automatically result in a “denied” flight status.



Correct, reliable and repeatable recovery system performance is absolute top priority from a safety point of view. Statistical data also concludes that namely recovery system failures are the major cause of abnormal “landings”.

### 3.8.3. OPTIONAL FLIGHT ELECTRONICS DEMONSTRATION

Teams are encouraged to have a setup to demonstrate the electronics and recovery system working routine in the FRR, either by a software routine that actuates the outputs of the flight computer and using LED indicators or buzzers or by a self-developed setup. This step is not mandatory, it is instead a recommendation for teams to detect some possible bugs and defects in their system.

## 4. STORED-ENERGY DEVICES

### 4.1. ENERGETIC DEVICE SAFING AND ARMING

All energetics shall be “safed” until the rocket is in the launch position, at which point they may be “armed”. An energetic device is considered safed when two separate events are necessary to release the energy of the system. An energetic device is considered armed when only one event is necessary to release the energy. For the purpose of this document, energetics are defined as all stored-energy devices – other than propulsion systems – that have reasonable potential to cause bodily injury upon energy release. The following table lists some common types of stored-energy devices and overviews and in which configurations they are considered non-energetic, safed, or armed.

*Table 2: Overviews and configurations of stored-energy devices.*

DEVICE CLASS	NON-ENERGETIC	SAFED	ARMED
Igniters/Squibs	Small igniters/squibs, nichrome, wire or similar	Large igniters with leads shunted	Large igniters with non-shunted leads
Pyrogens (e.g., black powder)	Very small quantities contained in non-shrapnel producing devices (e.g., pyro-cutters or pyro-valves)	Large quantities with no igniter, shunted igniter leads, or igniter(s) connected to unpowered avionics	Large quantities with non-shunted igniter or igniter(s) connected to powered avionics
Mechanical Devices (e.g., powerful springs)	De-energized/relaxed state, small devices, or captured devices (i.e., no jettisoned parts)	Mechanically locked and not releasable by a single event	Unlocked and releasable by a single event



Pressure Vessels	Non-charged pressure vessels	Charged vessels with two events required to open main valve	Charged vessels with one event required to open main valve
------------------	------------------------------	---	--

Although these definitions are consistent with the propulsion system arming definition provided in Section 2. of this document, this requirement is directed mainly at the energetics used by recovery systems and extends to all other energetics used in experiments, control systems, etc. Note that while Section 2.4.1. requires propulsion systems to be armed only after the launch rail area is evacuated to a specified distance, this requirement permits personnel to arm other stored-energy devices at the launch rail.

#### 4.1.1. ARMING DEVICE ACCESS

All energetic device arming features shall be externally accessible/controllable. This does not preclude the limited use of access panels which may be secured for flight while the vehicle is in the launch position.

#### 4.1.2. ARMING DEVICE LOCATION

All energetic device arming features shall be located on the airframe such that any inadvertent energy release by these devices will not impact personnel arming them. For example, the arming key switch for an energetic device used to deploy a hatch panel shall not be located at the same airframe clocking position as the hatch panel deployed by that charge.

Furthermore, it is highly recommended that the arming mechanism is accessible from ground level, without the use of ladders or other elevation devices, when the rocket is at a vertical orientation on the launch rail. If this requirement is considered early in the design process, implementing the arming devices in the lower section of the rocket is easy, while also mitigating the need for risky or hazardous arming procedures at a height.

### 4.2. SRAD PRESSURE VESSELS

The following requirements concern design and verification testing of SRAD and modified COTS pressure vessels. Unmodified COTS pressure vessels utilized for other than their advertised specifications will be considered modified, and subject to these requirements. SRAD (including modified COTS) rocket motor propulsion system combustion chambers are included as well but are exempted from the relief device requirement.



#### **4.2.1. RELIEF DEVICE**

SRAD pressure vessels shall implement a relief device, set to open at no greater than the proof pressure specified in the following requirements. SRAD (including modified COTS) rocket motor propulsion system combustion chambers are exempted from this requirement.

#### **4.2.2. DESIGNED BURST PRESSURE FOR METALLIC PRESSURE VESSELS**

SRAD and modified COTS pressure vessels constructed entirely from isotropic materials (e.g., metals) shall be designed to a burst pressure no less than 2 times the maximum expected operating pressure, where the maximum operating pressure is the maximum pressure expected during pre-launch, flight, and recovery operations.

#### **4.2.3. DESIGNED BURST PRESSURE FOR COMPOSITE PRESSURE VESSELS**

All SRAD and modified COTS pressure vessels either constructed entirely from non-isotropic materials (e.g., fibre reinforced plastics (FRP), composites) or implementing composite overwrap of a metallic vessel (i.e., composite overwrapped pressure vessels (COPV)), shall be designed to a burst pressure no less than 3 times the maximum expected operating pressure, where the maximum operating pressure is the maximum pressure expected during pre-launch, flight, and recovery operations.

#### **4.2.4. SRAD PRESSURE VESSEL TESTING**

Teams shall comply with all rules, regulations, and best practices imposed by the authorities at their chosen test location(s). The following requirements concern design and verification testing of SRAD and modified COTS pressure vessels. Unmodified COTS pressure vessels utilized for other than their advertised specifications will be considered modified, and subject to these requirements. SRAD (including modified COTS) rocket motor propulsion system combustion chambers are included as well.

##### **4.2.4.1. PROOF PRESSURE TESTING**

SRAD and modified COTS pressure vessels shall be proof pressure tested successfully (without significant anomalies) to 1.5 times the maximum expected operating pressure for no less than twice the maximum expected system working time, using the intended flight article(s) (e.g., the pressure vessel(s) used in proof testing must be the same one(s) flown at EuRoC). The maximum system working time is defined as the maximum uninterrupted time duration the vessel will remain pressurized during pre-launch, flight, and recovery operations (which for example could be hours for self-pressurized nitrous oxide propellant systems).



The test results and a statement of a successful test, complete with dates and signatures (at least three) are considered mandatory deliverable and annexed to the Technical Report.

The described annex may be amended to the Technical Report, as results become available, up to the day final deadline for delivery of the Technical Report. Failure to deliver this annex will automatically result in a “denied” flight status.

The pressure testing is an important factor in instilling confidence in the structural strength and integrity of the flown pressure vessels. Since liquid propellant loading onto hybrid or bi-liquid propelled flight vehicles will in the majority of cases involve manual loading, there will be times where ground personnel will be in close proximity with pressurized systems. It is crucial that ground personnel safety is heightened by the use of proof pressure tested pressure vessels.

#### 4.2.4.2. OPTIONAL BURST PRESSURE TESTING

Although there is no requirement for burst pressure testing, a rigorous verification & validation test plan typically includes a series of both non-destructive (i.e., proof pressure) and destructive (i.e., burst pressure) tests. A series of burst pressure tests performed on the intended design will be viewed favourably; however, this will not be considered an alternative to proof pressure testing of the intended flight article.

## 5. ACTIVE FLIGHT CONTROL SYSTEMS

### 5.1. CONTROL FUNCTIONALITY

Launch vehicle active flight control systems may be implemented for pitch and/or roll stability augmentation, for aerodynamic "braking", guided recovery systems, precision landing or guided deployable loads.

Any active flight control system implemented in any part of the vehicle, must be clearly described in the Technical Report, as well as under any concept/design report/reviews. The organisers may make additional requests for information and draft unique requirements depending on the team's specific design implementation.

As for designated landing zones/coordinates, travel corridors, loitering zones, etc., these are until further notice decided on a case-by-case between the Range Safety Officer, Mission Control Officer and team's recovery specialists.



## 5.2. UNNECESSARY FOR STABLE FLIGHT

Launch vehicles implementing active flight controls shall be naturally stable without these controls being implemented (e.g., the launch vehicle may be flown with the Control Actuator System (CAS) — including any control surfaces — either removed or rendered inert and mechanically locked, without becoming unstable during ascent).

Attitude Control Systems (ACS) will serve only to mitigate the small perturbations which affect the trajectory of a stable rocket that implements only fixed aerodynamic surfaces for stability. Stability is defined in Section 8.3. of this document. The organisers may make additional requests for information and draft unique requirements depending on the team's specific design implementation.

## 5.3. DESIGNED TO FAIL SAFE

Control Actuator Systems should be designed to Fail Safe in any abnormal condition or during an active flight abort (if such functionality is implemented). This means disabling cold-gas thrusters, returning control surface deflections to neutral position, disabling thrust vectoring, or seeking to disable any control feature which will apply any kind of moment to the flight vehicle.

As for any actuators acting in a uniform, interlocked or mirrored fashion, which increases air drag without applying any moment to the flight vehicle (such as airbrakes) these should be attempted fully extended in a fault or abort scenario, to slow down the flight vehicle as quickly as possible. If within the capability of the Control Actuator System, pilot chutes and even main parachutes can be ejected, as soon as the vehicle forward velocity is low enough not to snap the parachute lines.

## 5.4. BOOST PHASE DORMANCY

Since all flight vehicles with Control Actuator Systems (guidance systems) are to be designed inherently passively stable at lift-off, CAS should not be needed until somewhat into the flight, performing minor course corrections thereafter. In enforcing a boost dormancy phase, any unexpected, erratic, or faulty CAS behaviour will take place far from the launch rail, minimizing the chances of putting EuRoC participants at risk.

For any CAS without demonstrated flight history, without a documented SW configuration control, the Boost Phase Dormancy ends at an altitude of no less than 1500 m AGL. The EuRoC officials can set the boost phase dormancy expiration criteria higher as seen fit and this parameter must be field-programmable.

For any CAS with a (limited) demonstrated flight history, the default Boost Phase Dormancy expiration criteria is an altitude of 500 m AGL, again subject to EuRoC officials assessment.



For any CAS with adequate demonstrated flight history, ample simulation models, SW configuration control, single-fault tolerant design/FMECA analysis, and a hardware implementation considered by EuRoC officials as of superior quality of engineering and implementation, the Boost Phase Dormancy expiration altitude may on a case-by-case basis be set as low as the end of the launch rail.

A special case exists for CAS capable of exerting only lengthwise roll-control of the flight vehicle:

- If the CAS is inducing “spin stabilization” of the flight vehicle (a constant angular velocity), the roll control system can be enabled at the end of the launch rail.
- If the CAS is used to cancel spin or bring the flight vehicle to a particular angular position, the control system must remain inactive until an altitude of 1500 m.

**Note:** The above two can be combined, with the same system inducing spin stabilization from the end of the launch rail until an altitude of 1500 m is reached, whereafter the control system can be used to de-spin the flight vehicle.

## 5.5. RECOMMENDED FLIGHT TRAJECTORY FOR ACTIVE CONTROL SYSTEMS

The EuRoC nominal flight vehicle target trajectory is to maintain a compass direction of  $133^\circ$  from the launch rail (straight down the centreline of the ballistic corridor), maintaining an azimuth angle identical to the launch rail (nominally  $84^\circ \pm 1^\circ$ ) until apogee.

It must be noted that there is no requirement for active control systems to be disabled at apogee. In the event of a complete failure to deploy recovery systems and deliberately breaking up the flight vehicle, the “controlled disposal point” is a point twice the downrange distance from the launch rail to apogee, still at a compass direction of  $133^\circ$  from the launch rail (still down the centreline of the ballistic corridor).

It is noted that the nominal flight trajectory is ground-fixed, allowing teams to implement high-altitude crosswind compensation, etc., to maintain the nominal trajectory over ground.

This target flight trajectory will mimic the intended nominal ballistic trajectory of a passively stable flight vehicle until apogee. It furthermore increases ground safety by ensuring a predictable flight path away from the spectator area, providing a predictable downrange apogee and increasing the chances of the flight vehicle staying within both the ballistic corridor and the safety zone, even in the event of a complete recovery failure.

## 5.6. ACTIVE FLIGHT CONTROL SYSTEM ELECTRONICS

Wherever possible, all active control systems should comply with requirements and goals for "redundant electronics" and "safety critical wiring" as recovery systems — understanding that in this case "initiation" refers CAS commanding rather than a recovery event. These requirements and goals



are defined in Sections 3.3. . and 3.6. ., respectively, of this document. Flight control systems are exempt from the requirement for COTS redundancy, given that such components are generally unavailable as COTS to the amateur high-power rocketry community.

As for all electronics, it is highly recommended to ensure easy and quick access to switches/connectors via an access panel on the airframe. Access panels should be positioned so they are reachable from ground level, ideally without ladders. Access panels shall be secured for flight.

## **5.7. ACTIVE FLIGHT CONTROL SYSTEM ENERGETICS**

All stored-energy devices used in an active flight control system (i.e., energetics) shall comply with the energetic device requirements defined in Section 4. of this document.

# **6. AIRFRAME STRUCTURES**

## **6.1. ADEQUATE VENTING**

Launch vehicles shall be adequately vented to prevent unintended internal pressures developed during flight from causing either damage to the airframe or any other unplanned configuration changes. Typically, a 3 mm to 5 mm hole is drilled in the booster section just behind the nosecone or payload shoulder area, and through the hull or bulkhead of any similarly isolated compartment/bay.

## **6.2. OVERALL STRUCTURAL INTEGRITY**

Launch vehicles will be constructed to withstand the operating stress and retain structural integrity under the conditions encountered during handling as well as rocket flight. The following requirements address some key points applicable to almost all amateur high-power rockets but are not exhaustive of the conditions affecting each unique design. Student teams are ultimately responsible for thoroughly understanding, analysing and mitigating their design's unique load set.

### **6.2.1. MATERIAL SELECTION**

PVC (and similar low-temperature polymers), Public Missiles Ltd. (PML) Quantum Tube components shall not be used in any structural (i.e., load bearing) capacity, most notably as load bearing eyebolts, launch vehicle airframes, or propulsion system combustion chambers.





### 6.2.2. LOAD BEARING EYEBOLTS AND U-BOLTS

All load bearing eyebolts shall be of the closed-eye, forged type — NOT of the open eye, bent wire type. Furthermore, all load bearing eyebolts and U-Bolts shall be steel or stainless steel. This requirement extends to any bolt and eye-nut assembly used in place of an eyebolt.

### 6.2.3. IMPLEMENTING COUPLING TUBES

Airframe joints which implement "coupling tubes" should be designed such that the coupling tube extends no less than one body calibre (1D) on either side of the joint — measured from the separation plane. This rule applies both for "half" couplings (e.g., nosecone – body tube/coupling tube) as well as for "full" couplings (e.g., body tube – coupling tube – body tube). See example in Figure 3 for clarity. Regardless of implementation (e.g., RADAX or other join types) airframe joints need to be "stiff" (i.e., prevent bending).

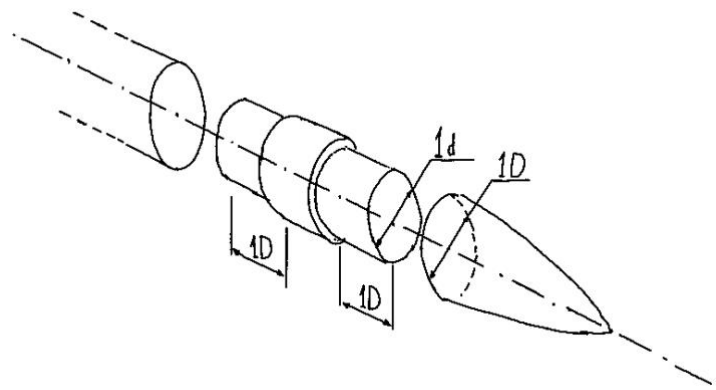


Figure 3: Examples for coupling tubes.

### 6.2.4. LAUNCH LUG MECHANICAL ATTACHMENT

Launch lugs (i.e., rail guides) should implement "hard points" for mechanical attachment to the launch vehicle airframe. These hardened/reinforced areas on the vehicle airframe, such as a block of wood installed on the airframe interior surface where each launch lug attaches, will assist in mitigating lug "tear outs" during operations.

The aft most launch lug shall support the launch vehicle's fully loaded launch weight while vertical.

At EuRoC, competition officials will require teams to lift their launch vehicles by the rail guides and/or demonstrate that the bottom guide can hold the vehicle's weight when vertical. This test needs to be completed successfully before the admittance of the team to Launch Readiness Review.



### 6.3. RF TRANSPARENCY

Any internally mounted RF transmitter, receiver or transceiver, not having the applicable antenna or antennas mounted externally on the airframe, shall employ "RF windows" in the airframe shell plating (typically glass fibre panels), enabling RF devices with antennas mounted inside the airframe, to transmit the signal through the airframe shell.

RF windows in the flight vehicle shell shall be a 360° circumference and be at least two body diameters in length. The internally mounted RF antenna(s) shall be placed at the midpoint of the RF window section, facilitating maximizing the azimuth radiation pattern.

RF transmitter, receivers or transceivers are not allowed to be mounted externally.

Please note, that even though a single downward facing antenna mounted on a stabilization fin near the engine seems like a good way to provide nearly a 360° radiation pattern from a single antenna without significant dead-zones. This is true at any point in time, except when the rocket engine is active. The ionized exhaust gas from the engine is highly disruptive to RF signals, so degradation or loss of link is to be expected.

As popular as carbon fibre is for the construction of strong and lightweight airframes, it is also conductive and will significantly shield and/or degrade RF signals, which is unacceptable. Externally mounted antennas often provide a more powerful and uniform radiation pattern but finds the flight vehicle body providing RF dead zones, meaning that at least two antennas on opposite sides of the airframe are advisable.

RF antennas shall be kept as far away as possible from wiring and metallic structural elements. Numerous examples of poor installation practice have at a great extent ruined telemetry and link performances. Teams are highly advised to follow best RF-practices.

### 6.4. IDENTIFYING MARKINGS

The team's Team ID (a number assigned by EuRoC prior to the competition event), project name, and academic affiliation(s) shall be clearly identified on the launch vehicle airframe. The Team ID especially, will be prominently displayed (preferably visible on all four quadrants of the vehicle, as well as fore and aft), assisting competition officials to positively identify the project hardware with its respective team throughout EuRoC.

### 6.5. OTHER MARKINGS

There are no requirements for airframe coloration or markings beyond those specified in Section 6.4. of this document. However, EuRoC offers the following recommendations to student teams: mostly white or lighter tinted colour (e.g., yellow, red, orange, etc.) airframes are especially conducive to



mitigating some of the solar heating experienced in the EuRoC launch environment. Furthermore, high-visibility schemes (e.g., high-contrast black, orange, red, etc.) and roll patterns (e.g., contrasting stripes, “V” or “Z” marks, etc.) may allow ground-based observers to track and record the launch vehicle’s trajectory with high-power optics more easily.

## **7. PAYLOAD**

### **7.1. PAYLOAD RECOVERY**

Payloads may be deployable or remain attached to the launch vehicle throughout the flight. Deployable payloads shall incorporate an independent recovery system, reducing the payload’s descent velocity to less than 9 m/s before it descends through an altitude of 450 m AGL.

All types of deployable payloads must be authorized by the EuRoC organisers prior to EuRoC. Deployable payloads without two-stage recovery systems (drogue and main chute, like the rockets) will be subjective to considerable drift during descent.

Note that deployable payloads implementing a parachute or parafoil based recovery system are not required to comply with the dual-event requirements described in Section 2. of this document, being allowed to utilize a single-stage 8-9m/s descent rate from apogee recovery system, subject to case-by-case EuRoC approval (the intent being to accommodate certain science/engineering packages requiring extended airborne mission time).

#### **7.1.1. PAYLOAD RECOVERY SYSTEM ELECTRONICS AND SAFETY CRITICAL WIRING**

Payloads implementing independent recovery systems shall comply with the same requirements and goals as the launch vehicle for "redundant electronics" and "safety critical wiring". These requirements and goals are defined in Sections 3.3. . and 3.6. . respectively.

#### **7.1.2. PAYLOAD RECOVERY SYSTEM TESTING**

Payloads implementing independent recovery systems shall comply with the same requirements and goals as the launch vehicle for "recovery system testing". These requirements and goals are defined in Section 3.8.

#### **7.1.3. DEPLOYABLE PAYLOAD LANDING SITE TRACKING REQUIRED**

It must be noted that deployable payloads are equivalent to flight vehicle bodies and sections, in that they can be difficult to locate after landing. All deployable payloads shall feature the same mandatory landing site tracking system as all rockets and rocket stages as specified in Section 3.5. of this document.



The landing site tracking locator ID must differ from the ID of the launch vehicle. Teams shall assign to each transmitter a call-sign respecting the format described in Sections 3.5.3. and 3.5.4.

## 7.2. PAYLOAD ENERGETIC DEVICES

All stored-energy devices (i.e., energetics) used in payload systems shall comply with the energetic device requirements defined in Section 4. of this document.

# 8. LAUNCH AND ASCENT TRAJECTORY REQUIREMENTS

## 8.1. LAUNCH AZIMUTH AND ELEVATION

Launch vehicles shall nominally launch at an elevation angle of  $84^{\circ} \pm 1^{\circ}$  and a launch azimuth defined by competition officials at EuRoC. Competition officials reserve the right to require certain vehicles' launch elevation be as low as  $70^{\circ}$  if flight safety issues are identified during pre-launch activities.

The tolerance expressed within the nominal launch azimuth is intended as nothing more than an expression of acceptable human error by the operator setting the launch rail elevation prior to launch.

## 8.2. LAUNCH STABILITY AND ADEQUATE RAIL TAKE-OFF VELOCITY

Launch vehicles shall have sufficient velocity upon "departing the launch rail" to ensure they will follow predictable flight paths. In lieu of detailed analysis, a rail departure velocity of at least 30 m/s is generally acceptable. By exception, a team may request to use detailed analysis to prove stability is achieved at a lower rail departure velocity down to 25 m/s, either theoretically (e.g., computer simulation) or empirically (e.g., flight testing). The 30m/s lower take-off velocity is a requirement and not a guideline. Rail take-off velocities in the range of 25-30m/s are to be considered rare exceptions.

Teams, particularly those with hybrid and liquid propulsion plants, should design their propulsion plants with ample (or even considerable) power margin. An over-powered propulsion system is preferable to an under-powered propulsion system.

Teams shall comply with all rules, regulations, and best practices imposed by the authorities at their chosen test location(s). Departing the launch rail is defined as the first instant in which the launch vehicle becomes free to move about the pitch, yaw, or roll axis. This generally occurs at the instant the last rail guide forward of the vehicle's centre of gravity (CG) separates from the launch rail.

The requirements for team provided launch rails are defined in Section 10. of this document.



### 8.3. ASCENT STABILITY

Launch vehicles shall remain "stable" for the entire ascent. Stable is defined as maintaining a static stability margin of at least 1.5 calibres throughout the whole flight phase (upon leaving the launch rail), regardless of CG movement due to depleting consumables and shifting centre of pressure (CP) location due to wave drag effects (which may become significant as low as 0.5 Mach).

### 8.4. OVER-STABILITY

All launch vehicles should avoid becoming "over-stable" during their ascent. A launch vehicle may be considered over-stable with a static margin significantly greater than 2 body calibres (e.g., greater than 6 body calibres).

## 9. EUROCC LAUNCH SUPPORT EQUIPMENT

### 9.1. LAUNCH RAILS

EuRoC will provide standardised launch rails for the teams that do not intend to bring their own launch rail. The vehicle is guided by a 50 mm x 50 mm cross-section aluminium rail by Kanya (see Figure 4 for details) The launch rail length is 12 m and the launch rail inclination usually  $84^{\circ} \pm 1^{\circ}$  to vertical, which may be lowered on a case-by-case basis if the EuRoC officials deem it necessary. For details on the launch lugs, please see Section 6.2.4. .

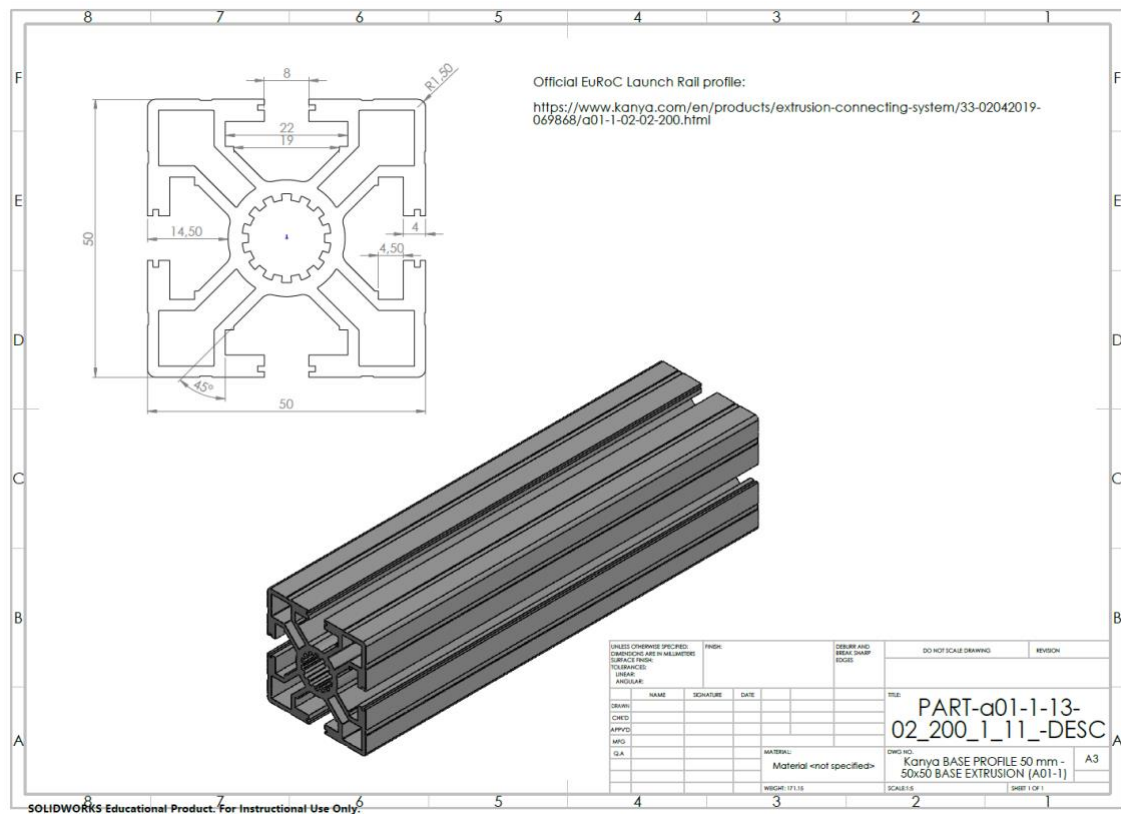
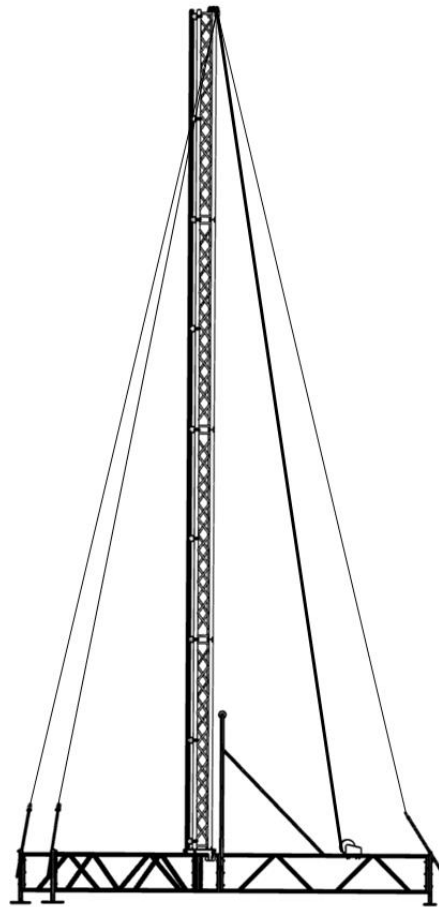


Figure 4: EuRoC launch rail profile.



*Figure 5: EuRoC launch rail fully assembled.*

### 9.1.1. LAUNCH RAIL FIT CHECK

All teams shall perform a “launch rail fit check” as a part of the flight preparations (the Flight Readiness Review), before going to the launch range. This requirement is particularly important if a team is not bringing their own launch rail, but instead relying on EuRoC provided launch rails. Teams shall provide their own bottom “spacer” to define their vehicles’ vertical position on the rail.

Arriving at the launch rails, only then discovering that a team's launch lugs does not fit the launch rail, will be considered gross negligence by EuRoC officials. The launch rail fit check will ensure that such surprises are not encountered on the launch rails, causing delays and loss of launch opportunities.

**Note:** The launch rail fit check can only be done in the presence of EuRoC officials. Teams cannot use the EuRoC launch rails without permission, any launch rail related activity shall be duly authorised by EuRoC officials.



## 9.2. EUROC-PROVIDED LAUNCH CONTROL SYSTEM

EuRoC will provide a Launch Control System. The system will be a Wilson F/X Wireless Launch Control System or equivalent.

The Wilson F/X wireless Launch Control System with one LCU-64x launch control unit and two PBU-8w encrypted pad relay boxes (more details on Wilson F/X Digital Launch Control Systems may be found on the Wilson F/X website: [www.wilsonfx.com](http://www.wilsonfx.com)).

## 10. TEAM-PROVIDED LAUNCH SUPPORT EQUIPMENT

### 10.1. EQUIPMENT PORTABILITY

If possible/practicable, teams should make their launch support equipment man-portable over a short distance (a few hundred metres). Environmental considerations at the launch site permit only limited vehicle use beyond designated roadways, campgrounds, and basecamp areas.

### 10.2. LAUNCH RAIL ELEVATION

Team provided launch rails shall implement the nominal launch elevation specified in Section 7. of this document and, if adjustable, not permit launch at angles either greater than the nominal elevation or lower than 70°.

### 10.3. OPERATIONAL RANGE

All team provided launch control systems shall be electronically operated and have a maximum operational range of no less than 650 metres from the launch rail. The maximum operational range is defined as the range at which launch may be commanded reliably.

### 10.4. FAULT TOLERANCE AND ARMING

All team provided launch control systems shall be at least single fault tolerant by implementing a removable safety interlock (i.e., a jumper or key to be kept in possession of the arming crew during arming) in series with the launch switch. 10.5. Appendix C: of this document provides general guidance on assuring fault tolerance in amateur high-power rocketry launch control systems.





## 10.5. SAFETY CRITICAL SWITCHES

All team provided launch control systems shall implement ignition switches of the momentary, normally open (also known as "dead man") type so that they will remove the signal when released. Mercury or "pressure roller" switches are not permitted anywhere in team provided launch control systems.



## APPENDIX A: ACRONYMS, ABBREVIATIONS & TERMS

<b>AA</b>	Actual Apogee
<b>ACS</b>	Attitude Control Systems
<b>AGL</b>	Above Ground Level
<b>APCP</b>	Ammonium Perchlorate Composite Propellant
<b>CAS</b>	Control Actuator System
<b>CATS</b>	Control and Telemetry Systems
<b>COPV</b>	Composite Overwrapped Pressure Vessels
<b>COTS</b>	Commercial of-the-shelf
<b>DTEG</b>	Design, Test and Evaluation Guide
<b>EuRoC</b>	European Rocketry Challenge
<b>FRP</b>	Fibre Reinforced Plastics
<b>FRR</b>	Flight Readiness Review
<b>GPS</b>	Global Positioning System
<b>H</b>	Hybrid
<b>L</b>	Liquid
<b>LOX</b>	Liquid Oxygen
<b>LRR</b>	Launch Readiness Review
<b>P</b>	Points
<b>PPE</b>	Personal Protective Equipment
<b>RF</b>	Radio Frequency
<b>S</b>	Solid
<b>SRAD</b>	Student Researched & Developed
<b>TA</b>	Target Apogee
<b>TEB</b>	Technical Evaluation Board



## APPENDIX B: GRADING CRITERIA

This section aims at giving the details for grading the participating teams of EuRoC in accordance with Section 11. of the EuRoC Rules & Requirements document. In the following sections teams can find all the details of the different criteria to be evaluated in each of the competition categories with an example of the grading scale in the table below.

Table 3: Example of the grading scale

GRADE	
2	exceptional
1	above average
0	average
-1	below average
2	poor

APOGEE (FOR FLIGHT PERFORMANCE)	
Apogee	see $P_{TA}AA \square = a \cdot -1 \cdot \cos\left(\frac{AA \cdot \pi}{TA}\right) + 1210$ Eq. 1

### B.1. TECHNICAL REPORT

Table 4: Technical report grading criteria.

CRITERION	MAX. POINTS	RELATIVE	DETAILS
Correctness	40	20%	Grammar, spelling, typing errors ("typos"), punctuation, sentence structure
			Correct use of scientific terms, units, dimensions, consistency, and usefulness of significant digits
			Technical clarity and disambiguation, correctness of scientific statements regarding general scientific knowledge
			Coherent stylistic appearance in terms of font, font size, style elements, colours, paragraphs, headlines, sufficient resolution of figures, presence of figure axis labels, clear and readable graphs/tables, etc.

CRITERION	MAX. POINTS	RELATIVE	DETAILS
-----------	-------------	----------	---------



Completeness	40	20%	Contains all required contents according to the requirements in a complete but concise fashion
--------------	----	-----	--

CRITERION	MAX. POINTS	RELATIVE	DETAILS
Analysis	120	60%	Explanation of key-design decisions, including trade-space analysis description (e.g. why was one option chosen over the other), constraints, and decision rational
			Clarity, understandability, and thoughtfulness in description of system architecture and mission concept of operations
			Discussion of key verification & validation tests performed on final design and possible previous designs, demonstrate complete and valid conclusions drawn from the results
			Appropriate use of tables, figures, and appendices to clearly organize and communicate information to the reader
			Quality, thoughtfulness, usefulness, and practicability of risk assessments, hazard analysis, checklists, technical drawings

## B.2. VEHICLE DESIGN

Table 5: Vehicle design grading criteria.

CRITERION	MAX. POINTS	RELATIVE	DETAILS
Design Challenges	75	30%	Selection and implementation of challenging and novel design features, in one or more particular aspects (e.g. active control, guidance, staging, propulsion, etc. ) and development of the technology necessary for achieving a successful implementation

CRITERION	MAX. POINTS	RELATIVE	DETAILS
Strategic Design Decisions	75	30%	Demonstration of a clear, achievable strategic vision for how challenges were selected to advance strategic goals, mirrored by the project's design implementation



			Degree of strategic consideration given to the design and inclusion of COTS and SRAD in the project, also in regard in keeping in line with the teams' articulated strategic vision
			Manufacturing methods used in SRAD aspects of the project, (e.g., additive manufacturing), are generally appropriate for the intended use and well understood by the team. Understanding extends not only to how the method works, but also its impact on project timelines, cost, and physical performance.

CRITERION	MAX. POINTS	RELATIVE	DETAILS
Competency of Design	50	20%	All features of the project hardware reflect strong competency in the physical principals governing the design
			Robustness of design characteristics, decreasing the design's sensitivity to reasonably expected variations in "real-world" operations
			Overall system engineering discipline maintained throughout development (e.g. not having any features which are both critical systems, and yet clearly implemented as "afterthoughts" to the intended system)

CRITERION	MAX. POINTS	RELATIVE	DETAILS
Design Implementation	50	20%	Design quality enabling operation as intended without risks or safety endangerment
			Implemented challenging and novel design features performance and added-value during operations
			SRAD systems performance during operations

### B.3. TEAM EFFORT

Table 6: Team effort grading criteria

CRITERION	MAX. POINTS	RELATIVE	DETAILS
	60	30%	Deposit Fee



Deliverables (correct, complete, timely)	Technical Questionnaire
	Concept Report
	Design Report (if applicable; if not applicable = 2)
	Video Presentation
	Technical Report
	Trajectory Simulation
	Proof of Insurance
	Waiver
	Final Team Composition

CRITERION	MAX. POINTS	RELATIVE	DETAILS
Organization, Operation, Communication	80	40%	Clear, open, honest, reliable, timely, and efficient communication in written and spoken word prior and during the event
			Organization and Reliability of the Team, e.g. team is present in time at the start of the event, team is reliable and in time for scheduled briefings and meetings (excluding spontaneous "snap-meetings"), clear responsibilities and roles within the team, clear points of contact towards the event officials
			Efficiency and preparedness of the team in prior to launch-site operations, including launch rail fit check, timely preparation for the scheduled launch readiness review without delays, timely transfer of equipment to the launch site
			Efficiency and preparedness of the team for launch-site operation, including dress-rehearsal of operations on launch day, general team readiness and preparedness for operations at the launch site, and preparedness towards unforeseen events ("Plan B")

CRITERION	MAX. POINTS	RELATIVE	DETAILS
-----------	-------------	----------	---------



Sportsmanship and Team Spirit	60	30%	Going above and beyond to assist fellow teams and the event organizers to assure the EuRoC is a productive, safe, and enjoyable experience for all involved, e.g. making themselves available to lend-a-hand whenever and however they can (whether they are asked to or not), being positive role models for their fellow teams, and generally being a "force for good" in every activity in which they involve themselves.
			Proverbial (or literal) smiles on their face, a school flag in their hand, and never lets either waiver throughout the event, show great pride in their work, learn from their mistakes, remain positive when things do not go their way, engage members of the public with respect and enthusiasm, and show respect for invited guests

#### B.4. FLIGHT PERFORMANCE

Points will be awarded according to the formula below and the following definitions: AA – actual apogee, TA – target apogee, P – points awarded, a – maximum number of points.

$$P_{TA}(AA) = a \cdot \left( \frac{(-1 \cdot \cos(\frac{AA \cdot \pi}{TA})) + 1}{2} \right)^{10} \quad \text{Eq. 1}$$

The points distribution is plotted for both target apogees in Figure 6 and Figure 7.

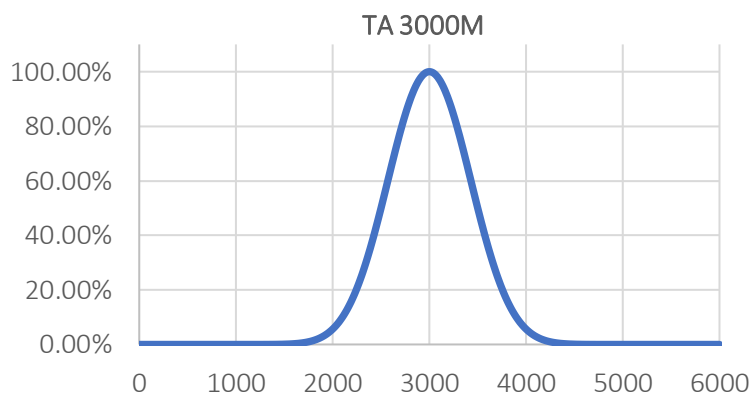


Figure 6: Points (P) awarded depending on actual apogee (AA) for a target apogee (TA) of 3000 m.

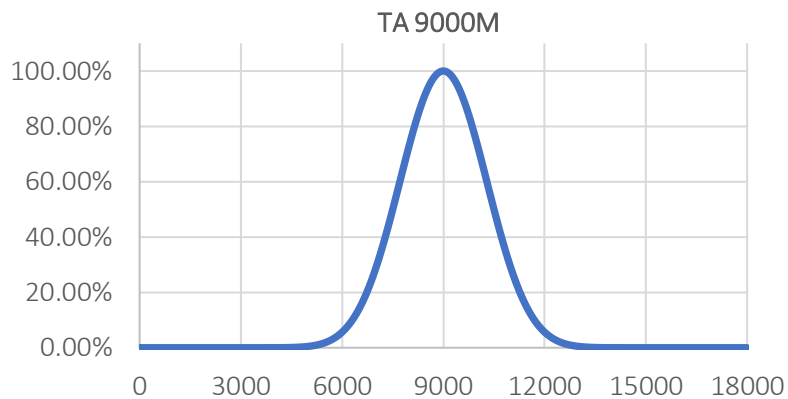


Figure 7: Points ( $P$ ) awarded depending on actual apogee ( $AA$ ) for a target apogee ( $TA$ ) of 9000 m.

Table 7: Flight performance grading criteria

CRITERION	MAX. POINTS	RELATIVE	DETAILS
Actual Apogee	175	50%	See $P_{TA}(AA) = a \cdot \left[ -1 \cdot \cos\left(\frac{AA \cdot \pi}{TA}\right) + 1 \right]$ Eq. 1 for more details.

CRITERION	MAX. POINTS	RELATIVE	DETAILS
Deployment	140	40%	Timeliness and quality of the deployment.

CRITERION	MAX. POINTS	RELATIVE	DETAILS
Postflight Vehicle State	35	10%	State of the launch vehicle upon its return to the designated basecamp area to determine the success of the recovery operation.





## APPENDIX C: FIRE CONTROL SYSTEM DESIGN GUIDELINES

### C.1. INTRODUCTION

The following section illustrates safe fire control system design best practices and philosophy to student teams participating in rocketry events. When it comes to firing (launch) systems for large amateur rockets, safety is paramount. This is a concept that everyone agrees with, but it is apparent that few truly appreciate what constitutes a “safe” firing system. Whether they have ever seen it codified or not, most rocketeers understand the basics:

- The control console should be designed such that two deliberate actions are required to fire the system;
- The system should include a power interrupt such that firing current cannot be sent to the firing leads while personnel are at the pad and this interrupt should be under the control of personnel at the pad.

These are good design concepts and if everything is working as it should they result in a perfectly safe firing system. But “everything is working as it should” is a dangerous assumption to make. Control consoles bounce around in the backs of trucks during transport. Cables get stepped on, tripped over, and run over. Switches get sand and grit in them. In other words, components fail. As such there is one more concept that should be incorporated into the design of a firing system:

*The failure of any single component should not compromise the safety of the firing system.*

### C.2. PROPER FIRE CONTROL SYSTEM DESIGN PHILOSOPHY

Let us examine a firing system that may at first glance appear to be simple, well designed, and safe (Figure 8). If everything is functioning as designed, this is a perfectly safe firing system, but let’s examine the system for compliance with proper safe design practices.

The control console should be designed such that two deliberate actions are required to launch the rocket. Check! There are actually three deliberate actions required at the control console: (1) insert the key, (2) turn the key to arm the system, (3) press the fire button.

The system should include a power interrupt such that ignition current cannot be sent to the firing leads while personnel are at the pad and this interrupt should be under control of personnel at the pad. Check and check! The firing relay effectively isolates the electric match from the firing power supply (battery) and as the operator at the pad should have the key in his pocket, there is no way that a person at the control console can accidentally fire the rocket.

But all of this assumes that everything in the firing system is working as it should. Are there any single component failures that can cause a compromise in the safety of this system? Yes. In a system that only has five components beyond the firing lines and e-match, three of those components can fail with potentially lethal results.

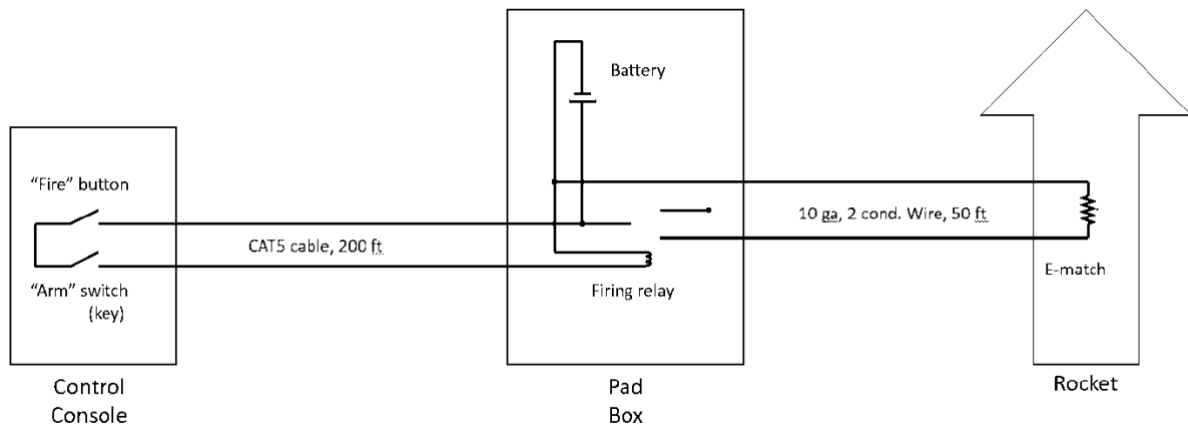


Figure 8: A simple high current fire control system.

**Firing Relay:** If the firing relay was stuck in the ON position: The rocket would fire the moment it was hooked to the firing lines. This is a serious safety failure with potentially lethal consequences as the rocket would be igniting with pad personnel in immediate proximity.

**Arming Switch:** If the arm key switch failed in the ON position simply pushing the fire button would result in a fired rocket whether intentional or not. This is particularly concerning as the launch key – intended as a safety measure controlled by pad personnel – becomes utterly meaningless. Assuming all procedures were followed, the launch would go off without a hitch. Regardless, this is a safety failure as only one action (pressing the fire button) would be required at the control console to launch the rocket. Such a button press could easily happen by accident. If personnel at the pad were near the rocket at the time we are again dealing with a potentially lethal outcome

**CAT5 Cable:** If the CAT5 cable was damaged and had a short in it the firing relay would be closed and the rocket would fire the moment it was hooked to the firing lines. This too is a potentially lethal safety failure.

Notice that all three of these failures could result in the rocket being fired while there are still personnel in immediate proximity to the rocket. A properly designed firing system does not allow single component failures to have such drastic consequences. Fortunately, the system can be fixed with relative ease.

Consider the revised system (Figure 9). It has four additional features built into it:

- (1) a separate battery to power the relay (as opposed to relying on the primary battery at the pad),
- (2) a flip cover over the fire button,
- (3) a lamp/buzzer in parallel with the firing leads (to provide a visual/auditory warning in the event that voltage is present at the firing lines), and
- (4) a switch to short-out the firing leads during hook up (pad personnel should turn the shunt switch ON anytime they approach the rocket).

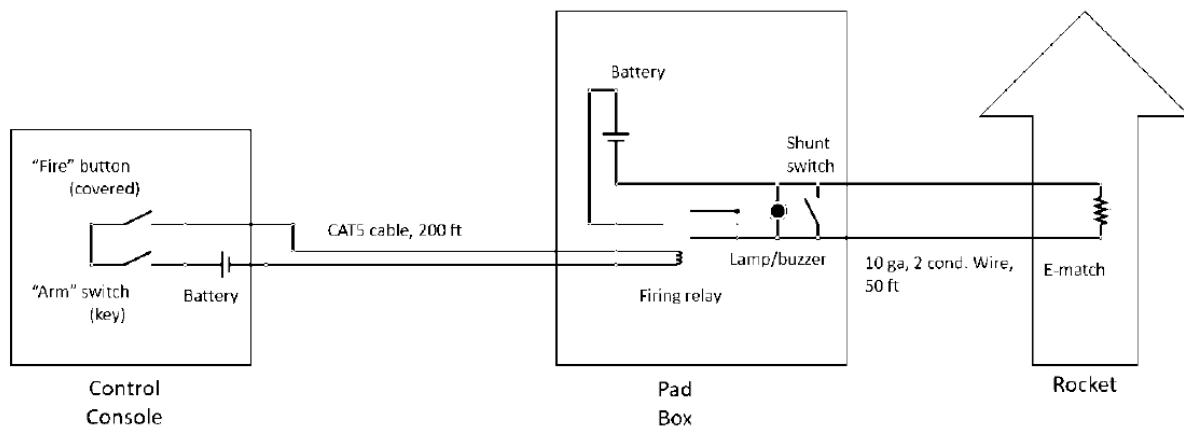


Figure 9: An improved high current fire control system.

In theory, these simple modifications to the previous firing circuit have addressed all identified single point failures in the system. The system has 8 components excluding the firing lines and e-match (part of the rocket itself). Can the failure of any of these components cause an inadvertent firing? That is the question. Let us examine the consequences of the failure of each of these components.

**Fire Button:** If the fire button fails in the ON position, there are still two deliberate actions at the control console required to fire the rocket. (1) The key must be inserted into the arming switch, and (2) the key must be rotated. The firing will be a bit of a surprise, but it will not result in a safety failure as all personnel should have been cleared by the time possession of the key is transferred to the Firing Officer.

**Arm Switch:** If the arm switch were to fail in the ON position, there are still two deliberate actions at the control console required to fire the rocket. (1) The cover over the fire button would have to be removed, and (2) the fire button would have to be pushed. This is not an ideal situation as the system would appear to function flawlessly even though it is malfunctioning and the key in the possession of personnel at the launch pad adds nothing to the safety of the overall system. It is for this reason that the shunting switch should be used. Use of the shunting switch means that any firing current would be dumped through the shunting switch rather than the e-match until the pad personnel are clear of the rocket. Thus, personnel at the pad retain a measure of control even in the presence of a malfunctioning arming switch and grossly negligent use of the control console.

**Batteries:** If either battery (control console or pad box) fails, firing current cannot get to the e-match either because the firing relay does not close or because no firing current is available. No fire means no safety violation.

**CAT5 Cable:** If the CAT5 cable were to be damaged and shorted, the system would simply not work as current intended to pull in the firing relay would simply travel through the short. No fire means no safety violation.



**Firing Relay:** If the firing relay fails in the ON position the light/buzzer should alert the pad operator of the failure before he even approaches the pad to hook up the e-match.

**Shunt switch, Lamp/Buzzer:** These are all supplementary safety devices. They are intended as added layers of safety to protect and/or warn of failures of other system components. Their correct (or incorrect) function cannot cause an inadvertent firing.

Is this a perfect firing system? No. There is always room for improvement. Lighted switches or similar features could be added to provide feedback on the health of all components. Support for firings at multiple launch pads could be included. Support for the fuelling of hybrids and/or liquids could be required. A wireless data link could provide convenient and easy to set up communications at greater ranges. The list of desired features is going to be heavily situation dependent and is more likely to be limited by money than good ideas.

Hopefully the reader is getting the gist: The circuit should be designed such that no single equipment failure can result in the inadvertent firing of the e-match and thus, the rocket motor. Whether or not a particular circuit is applicable to any given scenario is beside the larger point that in the event of any single failure a firing system should always fail safe and never fail in a dangerous manner. No matter how complicated the system may be, it should be analysed in depth and the failure of any single component should never result in the firing of a rocket during an unsafe range condition. Note that this is the bare minimum requirement; ideally, a firing system can handle multiple failures in a safe manner.



## APPENDIX D: FLIGHT READINESS REVIEW CHECKLIST

Table 8: Flight Readiness Review checklist.

SECTION	DESCRIPTION	ACTIONS TO BE TAKEN
<b>PROPULSION SYSTEMS</b>		
Checklist	Upon request, the flier should provide the inspector with hardcopy checklist procedures for the propulsion system's safe handling, assembly, disassembly, and operation (both nominal and off-nominal/contingency flows) – including self-inspection/verification steps which make individual team members accountable to one another for having completed the preceding process(es).	Simple confirmation Inspection on site
Non-toxic Propellants	Launch vehicles entering EuRoC shall use non-toxic propellants. Ammonium perchlorate composite propellant (APCP), potassium nitrate and sugar (also known as "rocket candy"), nitrous oxide, liquid oxygen (LOX), hydrogen peroxide, kerosene, propane, alcohol, and similar substances, are all considered non-toxic. Toxic propellants are defined as those requiring breathing apparatus, unique storage and transport infrastructure, extensive personal protective equipment (PPE), etc. Homemade propellant mixtures containing any fraction of toxic propellants are also prohibited.	Simple confirmation
Total Impulse	The sum of all rocket stages' impulse must either not exceed 40,960 newton-seconds, or the Flier must have previously consulted with EuRoC on provisions for launching a larger rocket.	Simple confirmation
Motor Retention	The design must provide for positive retention of the propulsion system within the airframe - leaving no possibility for the propulsion system to shift from its retaining device(s) and jettison itself.	Inspection on site Proof by reasoned argumentation
Thrust Structure	A "structural chain" that transfers the propulsion system thrust to various points on the rocket structure must exist and it must be capable of withstand these loads.	Inspection on site Proof by reasoned argumentation
Thrust Curve	Upon request, the flier must provide the inspector with hardcopy thrust curve data for each individual rocket motor or engine implemented.	Proof by calculation
<b>PROPULSION SYSTEM SAFING AND ARMING</b>		



<p>Pre-flight and Countdown Procedure</p>	<p>Upon request, the flier should provide the inspector with hardcopy checklist procedures for any of the propulsion system's unique final on-pad preparations, pre-flight, and launch (both nominal and off-nominal/abort/mishap flows) - including self-inspection/verification steps which make individual team members accountable to one another for having completed the preceding process(es).</p>	<p>Simple confirmation Inspection on site</p>
<p>Ground-start Ignition Circuit Arming</p>	<p>All ground-started propulsion system ignition circuits/sequences shall not be "armed" until all personnel are at least 15 m away from the launch vehicle. The provided launch control system satisfies this requirement by implementing a removable "safety jumper" in series with the pad relay box's power supply. The removal of this single jumper prevents firing current from being sent to any of the launch rails associated with that pad relay box. Furthermore, access to the socket allowing insertion of the jumper is controlled via multiple physical locks to ensure that all parties have positive control of their own safety.</p>	<p>Simple check</p>
<p>Air-start Ignition Circuit Arming</p>	<p>All upper stage (i.e., air-start) propulsion systems shall be armed by launch detection (e.g., accelerometers, zero separation force [ZSF] electrical shunt connections, break-wires, or other similar methods). Regardless of implementation, this arming function will prevent the upper stage from arming in the event of a misfire.</p>	<p>Proof by reasoned argumentation Inspection on site</p>
<p>Propellant Offloading After Launch Abort</p>	<p>Hybrid and liquid propulsion systems shall implement a means for remotely controlled venting or offloading of all liquid and gaseous propellants in the event of a launch abort.</p>	<p>Proof by reasoned argumentation</p>
<p>Air-start Ignition Circuit Electronics</p>	<p>All upper stage ignition systems shall comply with same requirements and goals for "redundant electronics" and "safety critical wiring" as recovery systems — understanding that in this case "initiation" refers to upper stage ignition rather than a recovery event.</p>	<p>Simple confirmation Inspection on site</p>
<p>Staging Ignition Commit Criteria</p>	<p>The electronics controlling the various staging events must inhibit staging if the rockets' flight profile deviates from predicted nominal behaviour.</p>	<p>Proof by reasoned argumentation</p>



Positive State Indication	Each independent set of electronics controlling staging events must provide sensory (i.e., visual or auditory) indication of its activation.	Simple confirmation Inspection on site
Special Consideration for "Drag Separation"	The electronics controlling stage ignition in design's implementing "drag-separation" must not be located in the separating stage - where premature separation could prevent ignition of the following stage.	Simple confirmation Inspection on site
<b>SRAD PROPULSION SYSTEM TESTING</b>		
Combustion Chamber Pressure testing	SRAD and modified COTS propulsion system combustion chambers shall be designed and tested according to the SRAD pressure vessel requirements defined in Section 4.2. . Note that combustion chambers are exempted from the requirement for a relief device.	Proof by previous testing
Hybrid and Liquid Propulsion System Tanking Testing	SRAD and modified COTS propulsion systems using liquid propellant(s) shall successfully (without significant anomalies) have completed a propellant loading and off-loading test in "launch-configuration", prior to the rocket being brought to the competition. This test may be conducted using either actual propellant(s) or suitable proxy fluids, with the test results to be considered a mandatory deliverable and an annex to the Technical Report, in the form of a loading and off-loading checklist, complete with dates, signatures (at least three) and a statement of a successful test. Failure to deliver this annex will automatically result in a "denied" flight status. Loading and unloading of liquid propellants must be a well-drilled, safe and efficient operation at the competition launch rails.	Proof by previous testing
Static Hot-fire testing	SRAD propulsion systems shall successfully (without significant anomalies) complete an instrumented (chamber pressure and/or thrust), full scale (including system working time) static hot-fire test prior to EuRoC. In the case of solid rocket motors, this test needs not to be performed with the same motor casing and/or nozzle components intended for use at the EuRoC (i.e., teams must verify their casing design, but are not forced to design reloadable/reusable motor cases). The test results and a statement of a successful test, complete with dates and signatures (at least three) are considered a mandatory deliverable and an annex to the	Proof by previous testing



	Technical Report. Failure to deliver this annex will automatically result in a “denied” flight status. See Section 2.6.6. for more information.	
<b>RECOVERY SYSTEMS AND AVIONICS</b>		
Checklist	Upon request, the flier must provide the inspector with hardcopy checklist procedures for the recovery system's safe handling, assembly, disassembly, and operation (both nominal and off-nominal/contingency flows) - including self-inspection/verification steps which make individual team members accountable to one another for having completed the preceding process(es).	Simple confirmation Inspection on site
Pre-flight and Countdown Procedure	Upon request, the flier must provide the inspector with hardcopy checklist procedures for any of the recovery system's unique final on-pad preparations, pre-flight, and launch (both nominal and off-nominal/abort/mishap flows) - including self-inspection/verification steps which make individual team members accountable to one another for having completed the preceding process(es).	Simple confirmation Inspection on site
Dual-event Parachute and Parafoil Recovery	Each independently recovered launch vehicle body, anticipated to reach an apogee above 450 m above ground level (AGL), shall follow a "dual-event" recovery operations concept, including an initial deployment event (e.g., a drogue parachute deployment; reefed main parachute deployment or similar) and a main deployment event (e.g., a main parachute deployment; main parachute un-reefing or similar). Independently recovered bodies, whose apogee is not anticipated to exceed 450 m AGL, are exempt and may feature only a single/main deployment event.	Proof by calculation Proof by reasoned argumentation
Inspect for Damage	If previously flown, any used parachutes, shock chords, and suspension lines must not exhibit signs of damage which threatens the safe recovery of the rocket.	Simple Confirmation Inspection on site
Initial Deployment Event	The initial deployment event shall occur at or near apogee, stabilize the vehicle's attitude (i.e., prevent or eliminate tumbling), and reduce its descent rate sufficiently to permit the main deployment event, yet not so much as to exacerbate wind drift. Any part, assembly or device, featuring an initial	Proof by reasoned argument (Deployment event) Proof by calculation (Descent rate) Proof by previous





	deployment event, shall result in a descent velocity of said item of 23-46 m/s.	testing (Descent rate)
Main Deployment Event	The main deployment event shall occur at an altitude no higher than 450 m AGL and reduce the vehicle's descent rate sufficiently to prevent excessive damage upon impact with ground. Any part, assembly or device, featuring a main deployment event, shall result in a descent velocity of said item of less than 9 m/s.	Proof by reasoned argumentation (Deployment event) Proof by calculation (Descent rate) Proof by previous testing (Descent rate)
Parachutes and Parafoils	Any parachutes or parafoils used must be rated for the weight of the vehicle and the expected conditions at deployment.	Proof by calculation
Safe Descent rate	Parachutes or parafoils intended for the final descent phase to the ground must not allow a descent rate that would represent a safety hazard.	Proof by calculation Proof by reasoned argumentation Proof by previous testing
Personal Safety	The arming/disarming process must not place the operator in the predicted path of hot gases, ejecta, or deployable devices which might result from an unintentional triggering event	Simple check
Activation Devices	The electronics controlling recovery events must be activated by externally accessible switches, and do not require any disassembly of the rocket to either activate or de-activate.	Simple confirmation
Positive State Indication	Each independent set of electronics controlling recovering events must provide sensory (i.e., visual or auditory) indication of its activation.	Simple confirmation Inspection on site
Acceleration Effects on Electronics	Heavy items - most notably batteries - must be adequately supported to prevent them becoming dislodged under anticipated flight loads.	Simple confirmation
Ejection Gas Protection	The recovery system shall implement adequate protection (e.g., fire-resistant material, pistons, baffles etc.) to prevent hot ejection gases (if implemented) from causing burn damage to retaining chords, parachutes, and other vital components as the specific design demands.	Simple confirmation Inspection on site
Parachute Swivel Links	The recovery system rigging (e.g., parachute lines, risers, shock chords, etc.) shall implement swivel links at connections to relieve torsion, as the specific design demands. This will mitigate the risk of torque	Simple confirmation Inspection on site



	loads unthreading bolted connections during recovery as well as parachute lines twisting up.	
Parachute Coloration and Markings	When separate parachutes are used for the initial and main deployment events, these parachutes should be visually highly dissimilar from one another. This is typically achieved by using parachutes whose primary colours contrast those of the other chute. This will enable ground-based observers to characterize deployment events more easily with high-power optics. Utilised parachutes should use colours providing a clear contrast to a blue sky and a grey/white cloud cover.	Simple confirmation
Non-parachute/Parafoil Recovery Systems	Teams exploring other recovery methods (i.e., non-parachute or parafoil based) shall mention them in the dedicated field of the Technical Questionnaire. The organisers may make additional requests for information and draft unique requirements depending on the team's specific design implementation.	Simple confirmation Inspection on site Proof by reasoned argumentation In-depth proofing needed
<b>REDUNDANT ELECTRONICS</b>		
Redundant COTS Recovery Electronics	At least one redundant recovery system electronics subsystem shall implement a COTS flight computer. To be considered COTS, the flight computer (including flight software) must have been developed and validated by a commercial third party.	Simple confirmation
Mandatory Official GPS Tracking and Tracking Systems	EuRoC will require teams to implement a common mandatory GPS tracking and locating device in all rocket systems featuring a dual-event deployment and recovery system.	Simple confirmation
Dissimilar Redundant Recovery Electronics	There is no requirement that the redundant/backup system be dissimilar to the primary; however, there are advantages to using dissimilar primary and backup systems. Such configurations are less vulnerable to any inherent environmental sensitivities, design, or production flaws affecting a particular component.	No action necessary
<b>SAFETY CRITICAL WIRING</b>		



Cable Management	All safety critical wiring shall implement a cable management solution (e.g., wire ties, wiring, harnesses, cable raceways) which will prevent tangling and excessive free movement of significant wiring/cable lengths due to expected launch loads. This requirement is not intended to negate the small amount of slack necessary at all connections/terminals to prevent unintentional de-mating due to expected launch loads transferred into wiring/cables at physical interfaces.	Simple confirmation Inspection on site
Secure Connections	All safety critical wiring/cable connections shall be sufficiently secure as to prevent de-mating due to expected launch loads. This will be evaluated by a "tug test", in which the connection is gently but firmly "tugged" by hand to verify it is unlikely to break free in flight.	Inspection on site
Cryo-compatible Wire Insulation	In case of propellants with a boiling point of less than -50°C any wiring or harness passing within the close proximity of a cryogenic device (e.g., valve, piping, etc.) or a cryogenic tank (e.g., a cable tunnel next to a LOX tank) shall utilize safety critical wiring with cryo-compatible insulation (i.e., Teflon, PTFE, etc.).	Inspection on site
Recovery System Energetic Devices	All stored-energy devices (aka energetics) used in recovery systems shall comply with the energetic device requirements defined in Section 4. of this document.	Simple confirmation
<b>RECOVERY SYSTEM TESTING</b>		
Ground Test Demonstration	All recovery system mechanisms shall be successfully (without significant anomalies) tested prior to EuRoC, either by flight testing, or through one or more ground tests of key subsystems. In the case of such ground tests, sensor electronics will be functionally included in the demonstration by simulating the environmental conditions under which their deployment function is triggered. The test results and a statement of a successful test, complete with dates and signatures (at least three) are considered a mandatory deliverable and annex to the Technical Report. Failure to deliver this annex will automatically result in a "denied" flight status.	Proof by previous testing



Optional Flight Test Demonstration	All recovery system mechanisms shall be successfully (without significant anomalies) tested prior to EuRoC, either by flight testing, or through one or more ground tests of key subsystems. While not required, a flight test demonstration may be used in place of ground testing. In the case of such a flight test, the recovery system flown will verify the intended design by implementing the same major subsystem components (e.g., flight computers and parachutes) as will be integrated into the launch vehicle intended for EuRoC (i.e., a surrogate booster may be used). The test results and a statement of a successful test, complete with dates and signatures (at least three) are considered a mandatory deliverable and annex to the Technical Report. Failure to deliver this annex will automatically result in a “denied” flight status.	No action necessary
<b>STORED-ENERGY DEVICES</b>		
Energetic Device Safing and Arming	All energetics shall be “safed” until the rocket is in the launch position, at which point they may be "armed". An energetic device is considered safed when two separate events are necessary to release the energy of the system. An energetic device is considered armed when only one event is necessary to release the energy. For the purpose of this document, energetics are defined as all stored-energy devices – other than propulsion systems – that have reasonable potential to cause bodily injury upon energy release. See Section 3. for more information.	Simple check
Arming Device Access	All energetic device arming features shall be externally accessible/controllable. This does not preclude the limited use of access panels which may be secured for flight while the vehicle is in the launch position.	Simple confirmation Inspection on site
Arming Device Location	All energetic device arming features shall be located on the airframe such that any inadvertent energy release by these devices will not impact personnel arming them. For example, the arming key switch for an energetic device used to deploy a hatch panel shall not be located at the same airframe clocking position as the hatch panel deployed by that charge. Furthermore, it is highly recommended that the arming mechanism is accessible from ground level, without the use of ladders or other elevation	Simple confirmation



	devices, when the rocket is at a vertical orientation on the launch rail.	
<b>SRAD PRESSURE VESSELS</b>		
Relief Device	SRAD pressure vessels shall implement a relief device, set to open at no greater than the proof pressure specified in the following requirements. SRAD (including modified COTS) rocket motor propulsion system combustion chambers are exempted from this requirement.	Proof by previous testing
Designed Burst Pressure for Metallic Pressure Vessels	SRAD and modified COTS pressure vessels constructed entirely from isentropic materials (e.g., metals) shall be designed to a burst pressure no less than 2 times the maximum expected operating pressure, where the maximum operating pressure is the maximum pressure expected during pre-launch, flight, and recovery operations.	Proof by calculation Proof by reasoned argumentation In-depth proofing needed
Designed Burst Pressure for Composite Pressure Vessels	All SRAD and modified COTS pressure vessels either constructed entirely from non-isentropic materials (e.g., fibre reinforced plastics; FRP; composites) or implementing composite overwrap of a metallic vessel (i.e., composite overwrapped pressure vessels; COPV), shall be designed to a burst pressure no less than 3 times the maximum expected operating pressure, where the maximum operating pressure is the maximum pressure expected during pre-launch, flight, and recovery operations.	Proof by calculation Proof by reasoned argumentation In-depth proofing needed
<b>SRAD PRESSURE VESSEL TESTING</b>		
Proof Pressure Testing	SRAD and modified COTS pressure vessels shall be proof pressure tested successfully (without significant anomalies) to 1.5 times the maximum expected operating pressure for no less than twice the maximum expected system working time, using the intended flight article(s) (e.g., the pressure vessel(s) used in proof testing must be the same one(s) flown at EuRoC). The maximum system working time is defined as the maximum uninterrupted time duration the vessel will remain pressurized during pre-launch, flight, and recovery operations. The test results and a statement of a successful test, complete with dates and signatures (at least three) are considered mandatory deliverable and annexed	Proof by previous testing



	to the Technical Report. Failure to deliver this annex will automatically result in a “denied” flight status.	
Optional Burst Pressure Testing	Although there is no requirement for burst pressure testing, a rigorous verification & validation test plan typically includes a series of both non-destructive (i.e., proof pressure) and destructive (i.e., burst pressure) tests. A series of burst pressure tests performed on the intended design will be viewed favourably; however, this will not be considered an alternative to proof pressure testing of the intended flight article.	No action necessary
<b>ACTIVE FLIGHT CONTROL SYSTEMS</b>		
Restricted Control Functionality	Launch vehicle active flight control systems shall be optionally implemented strictly for pitch and/or roll stability augmentation, or for aerodynamic "braking". Under no circumstances will a launch vehicle entered in EuRoC be actively guided towards a designated spatial target. The organisers may make additional requests for information and draft unique requirements depending on the team's specific design implementation.	Simple confirmation
Unnecessary for Stable Flight	Launch vehicles implementing active flight controls shall be naturally stable without these controls being implemented (e.g., the launch vehicle may be flown with the control actuator system [CAS] — including any control surfaces — either removed or rendered inert and mechanically locked, without becoming unstable during ascent). Attitude Control Systems (ACS) will serve only to mitigate the small perturbations which affect the trajectory of a stable rocket that implements only fixed aerodynamic surfaces for stability. The organisers may make additional requests for information and draft unique requirements depending on the team's specific design implementation.	Proof by reasoned argumentation Inspection on site
Designed to Fail Safe	Control Actuator Systems (CAS) shall mechanically lock in a neutral state whenever either an abort signal is received for any reason, primary system power is lost, or the launch vehicle's attitude exceeds 30° from its launch elevation. Any one of these conditions being met will trigger the fail-safe, neutral system state. A neutral state is defined as one which does not apply any moments to the	Proof by reasoned argumentation Inspection on site



	launch vehicle (e.g., aerodynamic surfaces trimmed or retracted, gas jets off, etc.).	
Boost Phase Dormancy	CAS shall mechanically lock in a neutral state until either the mission's boost phase has ended (i.e., all propulsive stages have ceased producing thrust), the launch vehicle has crossed the point of maximum aerodynamic pressure (i.e., max Q) in its trajectory, or the launch vehicle has reached an altitude of 6.000 m AGL. Any one of these conditions being met will permit the active system state. A neutral state is defined as one which does not apply any moments to the launch vehicle (e.g., aerodynamic surfaces trimmed or retracted, gas jets off, etc.).	Proof by reasoned argumentation Inspection on site
Active Flight Control System Electronics	Wherever possible, all active control systems should comply with requirements and goals for "redundant electronics" and "safety critical wiring" as recovery systems — understanding that in this case "initiation" refers CAS commanding rather than a recovery event. Flight control systems are exempt from the requirement for COTS redundancy, given that such components are generally unavailable as COTS to the amateur high-power rocketry community.	Simple confirmation
Active Flight Control System Energetics	All stored-energy devices used in an active flight control system (i.e., energetics) shall comply with the energetic device requirements defined in Section 4. of this document.	Simple confirmation
<b>AIRFRAME STRUCTURES</b>		
Adequate Venting	Launch vehicles shall be adequately vented to prevent unintended internal pressures developed during flight from causing either damage to the airframe or any other unplanned configuration changes. Typically, a 3 mm to 5 mm hole is drilled in the booster section just behind the nosecone or payload shoulder area, and through the hull or bulkhead of any similarly isolated compartment/bay.	Simple confirmation Inspection on site
<b>OVERALL STRUCTURAL INTEGRITY</b>		
Checklist	Upon request, the flier should provide the inspector with hardcopy checklist procedures for the rocket's assembly and integration for flight - including self-inspection/verification steps which make individual	Simple confirmation Inspection on site



	team members accountable to one another for having completed the preceding process(es).	
Material Selection	PVC (and similar low-temperature polymers), Public Missiles Ltd. (PML) Quantum Tube components shall not be used in any structural (i.e., load bearing) capacity, most notably as load bearing eyebolts, launch vehicle airframes, or propulsion system combustion chambers.	No action necessary (for stainless steel components) Simple confirmation
Load Bearing Eyebolts and U-bolts	All load bearing eyebolts shall be of the closed-eye, forged type — NOT of the open eye, bent wire type. Furthermore, all load bearing eyebolts and U-Bolts shall be steel or stainless steel. This requirement extends to any bolt and eye-nut assembly used in place of an eyebolt.	No action necessary (for stainless steel) Inspection on site
Implementing Coupling Tubes	Airframe joints which implement "coupling tubes" should be designed such that the coupling tube extends no less than one body calibre on either side of the joint — measured from the separation plane. Regardless of implementation (e.g., RADAX or other join types) airframe joints will be "stiff" (i.e., prevent bending).	Simple confirmation Proof by reasoned argumentation
Launch Lug Mechanical Attachment	Launch lugs (i.e., rail guides) should implement "hard points" for mechanical attachment to the launch vehicle airframe. These hardened/reinforced areas on the vehicle airframe, such as a block of wood installed on the airframe interior surface where each launch lug attaches, will assist in mitigating lug "tear outs" during operations. The aft most launch lug shall support the launch vehicle's fully loaded launch weight while vertical. At EuRoC, competition officials will require teams to lift their launch vehicles by the rail guides and/or demonstrate that the bottom guide can hold the vehicle's weight when vertical. This test needs to be completed successfully before the admittance of the team to Launch Readiness Review.	Inspection on site Proof by previous testing
Launch Rail Fit Check	All teams shall perform a "launch rail fit check" as a part of the flight preparations (the Launch Readiness Review), before going to the launch range. This requirement is particularly important if a team is not bringing their own launch rail, but instead relying on EuRoC provided launch rails.	Inspection on site





Rail Guide Attachment	The rail guides must be firmly attached to the rocket without evidence of cracking in the joints, and the aft most guide attachment must be sufficient to bear the rocket's entire mass when erected.	Inspection on site
Slip-fit Joints	Joints intended to separate in flight cannot become separated when loaded by their own weight alone, and the Flier should demonstrate cognizance of shear pin design (if implemented).	Proof by reasoned argumentation
Joint Stiffness	All joints - both separating and non-separating in flight - must be "stiff", so as to eliminate any visible airframe bending.	Inspection on site
Fin Attachment	The fins must be firmly attached to the rocket without evidence of cracking in the joints. ("Hairline" cracks may be acceptable if the fins are not loose or, if the fins are mounted using the "through-the-wall" [TTW] construction technique.	Inspection on site
Fin Stiffness	The fins must exhibit no shifting and minimal deflection (i.e., bending) when handled.	Inspection on site
Fin "Warpage"	The fins must exhibit little-to-no indication of damage due to moisture penetration or excessive thermal cycling during storage or transport - leading to out of tolerance dimensional changes in the part.	Inspection on site
<b>RF TRANSPARENCY</b>		
RF Window Location	<p>Any internally mounted RF transmitter, receiver or transceiver, not having the applicable antenna or antennas mounted externally on the airframe, shall employ "RF windows" in the airframe shell plating (typically glass fibre panels), enabling RF devices with antennas mounted inside the airframe, to transmit the signal though the airframe shell. RF windows in the flight vehicle shell shall be a 360° circumference and be at least two body diameters in length. The internally mounted RF antenna(s) shall be placed at the midpoint of the RF window section, facilitating maximizing the azimuth radiation pattern.</p> <p>RF transmitter, receivers or transceivers are not allowed to be mounted externally. Externally mounted antennas are allowed, but only if at least two antennas are mounted on opposite sides of the airframe, thus retaining circumferential symmetry and covering sufficient transmission area, transmitting or receiving identical signals.</p>	Simple confirmation



	As popular as carbon fibre is for the construction of strong and lightweight airframes, it is also conductive and will significantly shield and/or degrade RF signals, which is unacceptable.	
Identifying Markings	The team's Team ID (a number assigned by EuRoC prior to the competition event), project name, and academic affiliation(s) shall be clearly identified on the launch vehicle airframe. The Team ID especially, will be prominently displayed (preferably visible on all four quadrants of the vehicle, as well as fore and aft), assisting competition officials to positively identify the project hardware with its respective team throughout EuRoC.	No action necessary
Other Markings	There are no requirements for airframe coloration or markings beyond those specified in Section 6.4. . of this document. However, EuRoC offers the following recommendations to student teams: mostly white or lighter tinted colour (e.g., yellow, red, orange, etc.) airframes are especially conducive to mitigating some of the solar heating experienced in the EuRoC launch environment. Furthermore, high-visibility schemes (e.g., high-contrast black, orange, red, etc.) and roll patterns (e.g., contrasting stripes, "V" or "Z" marks, etc.) may allow ground-based observers to more easily track and record the launch vehicle's trajectory with high-power optics.	No action necessary
<b>PAYLOAD</b>		
Payload Mass	The launch vehicle shall carry no less than 1000 g of payload. Teams are responsible for conducting a "weigh-in" on site in the presence of the competition officials. Competition officials will accept payload weigh-ins as much as 5% (50 g) less than the specified minimum. If this requirement is not met, "nominal" flight status for the payload may be denied by the officials during FRR, resulting in an action item to increase payload mass.	Inspection on site



Payload recovery	<p>Payloads may be deployable or remain attached to the launch vehicle throughout the flight. Deployable payloads shall incorporate an independent recovery system, reducing the payload's descent velocity to less than 9 m/s before it descends through an altitude of 450 m AGL. Deployable payloads without two-stage recovery systems (drogue and main chute, like the rockets) will be subjective to considerable drift during descent.</p>	<p>Proof by calculation Proof by reasoned argumentation Proof by previous testing</p>
Payload Recovery System Electronics and Safety Critical Wiring	<p>Payloads implementing independent recovery systems shall comply with the same requirements and goals as the launch vehicle for "redundant electronics" and "safety critical wiring".</p>	<p>Inspection on site</p>
Payload Recovery System Testing	<p>Payloads implementing independent recovery systems shall comply with the same requirements and goals as the launch vehicle for "recovery system testing".</p>	<p>Simple confirmation</p>
Deployable Payload Landing Site Tracking Required	<p>It must be noted that deployable payloads are equivalent to flight vehicle bodies and sections, in that they can be difficult to locate after landing. All deployable payloads shall feature the same mandatory landing site tracking system as all rockets and rocket stages as specified in Section 3.5. The landing site locator ID must comply with the call-sign requirements defined in Sections 3.5.3. and 3.5.4.</p>	<p>Simple confirmation</p>
Payload Energetic Devices	<p>All stored-energy devices (i.e., energetics) used in payload systems shall comply with the energetic device requirements defined in Section 4. of this document.</p>	<p>Simple confirmation</p>
<b>LAUNCH AND ASCENT TRAJECTORY REQUIREMENTS</b>		
Launch Azimuth and Elevation	<p>Launch vehicles shall nominally launch at an elevation angle of <math>84^{\circ} \pm 1^{\circ}</math> and a launch azimuth defined by competition officials at EuRoC. Competition officials reserve the right to require certain vehicles' launch elevation be as low as <math>70^{\circ}</math>, if flight safety issues are identified during pre-launch activities.</p>	<p>Simple check</p>



Launch Stability	Launch vehicles shall have sufficient velocity upon "departing the launch rail" to ensure they will follow predictable flight paths. In lieu of detailed analysis, a rail departure velocity of at least 30 m/s is generally acceptable. Alternatively, the team may use detailed analysis to prove stability is achieved at a lower rail departure velocity 20 m/s either theoretically (e.g., computer simulation) or empirically (e.g., flight testing).	Proof by calculation
Ascent Stability	Launch vehicles shall remain "stable" for the entire ascent. Stable is defined as maintaining a static margin of at least 1.5 to 2 body calibres, regardless of CG movement due to depleting consumables and shifting centre of pressure (CP) location due to wave drag effects (which may become significant as low as 0.5 Mach). Not falling below 2 body calibres will be considered nominal, while falling below 1.5 body calibres will be considered a loss of stability.	Proof by calculation
Over-stability	All launch vehicles should avoid becoming "over-stable" during their ascent. A launch vehicle may be considered over-stable with a static margin significantly greater than 2 body calibres (e.g., greater than 6 body calibres).	Proof by calculation
Flight Simulation	Upon request, the flier should either provide a hard copy, or demonstrate on a portable computer, a 3-degree-of-freedom (3DoF) simulation (or better) of the rocket's nominal trajectory.	In-depth proofing needed
Fin Alignment	The fins should be mounted parallel to the roll axis of the rocket, or (if canted or otherwise roll inducing) the Flier must demonstrate cognizance of the predicted roll behaviour and its effects.	Inspection on site
Staging Event Sequence and Timing	Any delays implemented between staging events must not be so long as to significantly risk the rocket having "arced-over" into an unsafe orientation - typically by "gravity turn".	Proof by calculation
<b>TEAM-PROVIDED LAUNCH SUPPORT EQUIPMENT</b>		
Equipment Portability	If possible/practicable, teams should make their launch support equipment man-portable over a short distance (a few hundred metres). Environmental considerations at the launch site permit only limited vehicle use beyond designated roadways, campgrounds, and basecamp areas.	Simple confirmation



Launch Rail Elevation	Team provided launch rails shall implement the nominal launch elevation specified in Section 7. of this document and, if adjustable, not permit launch at angles either greater than the nominal elevation or lower than 70°.	Inspection on site
Operational Range	All team provided launch control systems shall be electronically operated and have a maximum operational range of no less than 650 metres from the launch rail. The maximum operational range is defined as the range at which launch may be commanded reliably.	No action necessary
Fault Tolerance and Arming	All team provided launch control systems shall be at least single fault tolerant by implementing a removable safety interlock (i.e., a jumper or key to be kept in possession of the arming crew during arming) in series with the launch switch.	Inspection on site
Safety Critical Switches	All team provided launch control systems shall implement ignition switches of the momentary, normally open (also known as "dead man") type so that they will remove the signal when released. Mercury or "pressure roller" switches are not permitted anywhere in team provided launch control systems.	Simple confirmation
<b>EQUIPMENT</b>		
Communication Equipment	All teams must bring any Personal Protection Equipment (PPE) required for all preparation- and launch activities. EuRoC does not have a supply of spare PPE. PPE includes, but is not limited to, safety goggles, gloves, safety shoes, hardhats, ear protection, cryo-protection, etc.	No action necessary
Personal Protection Equipment	All teams must bring any Personal Protection Equipment (PPE) required for all preparation- and launch activities. EuRoC does not have a supply of spare PPE. PPE includes, but is not limited to, safety goggles, gloves, safety shoes, hardhats, ear protection, cryo-protection, etc.	Simple confirmation
Field Equipment	All teams are encouraged to provide each participating team member with a suitable "field/day pack", which is kept close at hand (or worn) during launch days. Due to the possibility of strong sunlight and high temperatures even in October, some of these provisions are intended to get students through a hot and dry day in the field,	No action necessary



	while other provisions are intended to enable student teams to continue efficient operation after loss of daylight after a quick sun-down and a resulting sudden and significant drop in ambient temperature.	
--	---	--

Table 9: Legend for de-scoping FRR checklist.

LEGEND FOR DE-SCOPING FEEDBACK
This requirement is very important
This requirement is important
This requirement is of lesser importance

Table 10: Legend for actions to be taken on the FRR checklist.

ACTIONS TO BE TAKEN	
No action necessary	“I see you used stainless steel here. Okay, fine”
Simple confirmation	“Are you using non-toxic propellants?” – “Yes, we are”
Simple check	“Is everybody at least 15 m away when the ground-start ignition circuit is arming?” – “Okay now, yes”
Inspection on site	“Are all the critical wiring/cable connections sufficiently secured?” – “I will have a look, ah I see, yes”
Proof by reasoned argumentation	“Can you tell me about your process of offloading propellant in case of a launch abort?” – “Okay, sounds reasonable, this should work.”
Proof by previous testing	“Have you tested the pressure vessels to 1.5 the maximum expected operating pressure?” – “Okay, I will have a look at the results and understand if everything has been tested appropriately.”
Proof by calculation	“Regarding the launch stability, have you calculated the lower rail departure velocity? How did you do it? What is the result?” – “Okay, I see and understand the calculation, this will work then.”
In-depth proofing needed	“How does this design feature work?” – “Okay, so you are not certain, and I do not understand on site, so let us go to the CAD model and check.”